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BEHAVE: Fire Behavior Prediction and Fuel Modeling System — BURN Subsystem, Part 2

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INTRODUCTION

The BEHAVE fire behavior prediction and fuel modeling system is a set of interactive computer programs. BEHAVE provides mathematical prediction models in one easy-to-use package. This paper describes prediction capabilities that have been added to the system.

Since 1984, BEHAVE has been used by land managers for a variety of fire management needs. A user can tailor predictions to specific needs based on the resolution of the input and interpretation of the output. For example, windspeed might be measured on site for real-time prediction of wildfire behavior. On the other hand, windspeed can be assigned a range of values in order to make assessments for planning purposes. Example uses of BEHAVE predictions are determining appropriate suppression action, predicting the growth of a wilderness fire, prescribed fire planning, setting dispatch levels, and afterthe-fact predictions for an investigation.

This paper is the third in a series of papers that describe the BEHAVE system. Burgan and Rothermel (1984) described the FUEL subsystem of BEHAVE, used for designing custom fuel models. Andrews (1986) described the initial BURN subsystem, the operational fire behavior prediction part of BEHAVE. This paper covers additions that have been made to the BURN subsystem.

Part 1 of the BURN manual described the FIRE1 program. This paper is Part 2 of the BURN manual and describes additions to the FIRE1 program and the new FIRE2 program. The information in Part 1 is still valid. Worksheets for all modules in the FIRE1 and FIRE2 programs are in this manual (appendix B).

We assume that you are familiar with BEHAVE, specifically with the material in Part 1 of the BURN manual. References will be made to that paper (Andrews 1986) by page number (for example, Part 1, p. 23). As with Part 1, the emphasis of this paper is on description of the prediction models. You are responsible for supplying valid input and for properly interpreting output.

OVERVIEW OF THE BEHAVE SYSTEM

A diagram of the BEHAVE system design is shown in figure 1. The BURN subsystem previously consisted of only one program. It now has two, FIRE1 and FIRE2. The only reason for the split is to limit program size.

BEHAVE's "user-friendly" design makes it unnecessary to provide detailed instructions on how to run the programs. Annotated runs of the FIRE1 and FIRE2 programs are given in appendix A. Operation of all of the BEHAVE programs is based on keywords. A list of all keywords in the BURN subsystem and a brief description of each is shown in figure 2. Module keywords (DIRECT, SITE, SIZE, ...) are used to specify the prediction that is desired. Operation keywords (INPUT, LIST, CHANGE, RUN) are used to enter input and obtain output. Mode keywords (WORDY, TERSE, PAUSE, ...) are used to set a switch that remains in effect until you change it. Rescue keywords (KEY, HELP) should rescue you if you get mixed up.

All of the modules can be used independently. Some of them can also be linked to others as shown in figure 3. In that case, input and/or output is carried over from one module to the next.

Input/output sheets for all modules of the BURN subsystem are included in appendix B. In some cases, they are different from those given in Part 1. To avoid confusion, the date is at the bottom of each worksheet.

The Input/Output sheets give line numbers, item names, both English and metric units, comments, and one blank. These are information sheets and not worksheets. Most users will use computer printout to document runs rather than completing a worksheet. Custom worksheets can be designed as needed.

BEHAVE System Design

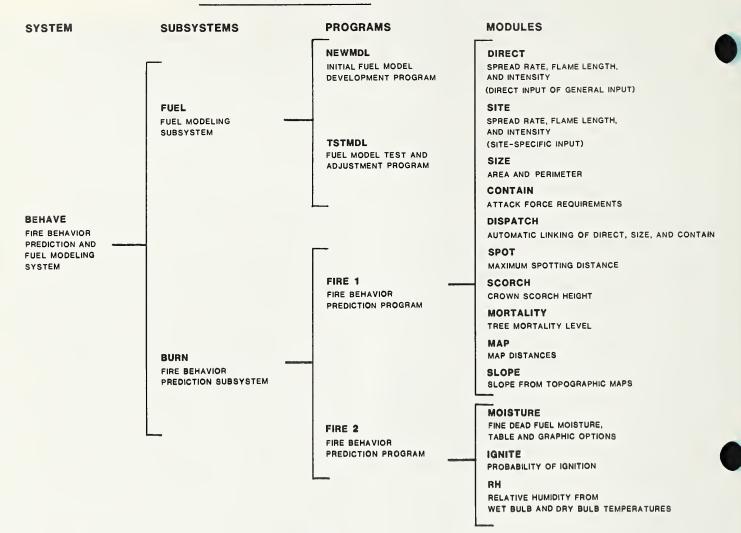
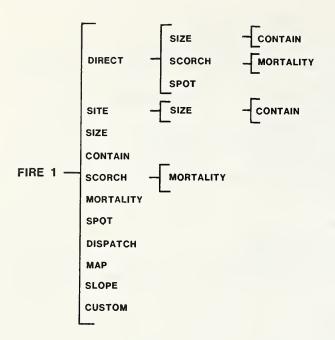


Figure 1—Subsystems, programs, and modules of the BEHAVE system.

FIRE1 only	
Module Keywords	
DIRECT	Accepts direct input of the basic values to calculate spread rate, flame length, and intensity.
SITE	Accepts site-specific input to calculate spread rate, flame length, and intensity. Fine dead fuel moisture is an intermediate value.
SIZE	Calculates area and perimeter of a point source fire.
CONTAIN	Calculates either line construction capabilities needed or final fire size.
DISPATCH	Automatically links DIRECT, SIZE, and CONTAIN
SPOT	Calculates maximum spotting distance from torching trees, a burning pile, or wind-driven surface fire.
SCORCH	Calculates crown scorch height
MORTALITY	Calculates level of tree mortality
MAP	Translates calculated distances to map distances
SLOPE	Calculates slope from topographic map measurements
CUSTOM	Specifies a custom fuel model file to be used or lists what is in a fuel model file
FIRE2 only	
Module Keywords	
MOISTURE	Calculates fine dead fuel moisture
IGNITE	Calculates probability of ignition
RH	Calculates relative humidity from wet bulb and dry bulb temperatures
FIRE1 and FIRE2	
Operation Keywords	
INPUT	Asks for all input of the current module
LIST	Lists current input values
CHANGE	Changes individual input values by line number
RUN	Does calculations and presents results
Mode Keywords	
WORDY	Gives extra messages and explanations throughout the run (default)
TERSE	Skips extra messages and explanations
PAUSE	Limits display to at most 24 lines at a time for a video display terminal (default)
NOPAUSE	No pause in display for a terminal with hard-copy output
LOG	Writes results of LIST, RUN and COMMENT to a file to be printed at a later time
NOLOG	turns off the LOG option (default)
ENGLISH	English units (default)
METRIC	Metric units
PERCENT	Slope in percent (default)
DEGREES	Slope in degrees
Rescue Keywords	
KEY	Prints the keywords that are allowed at the current point along with a brief description of each
HELP	Tells you where you are in the program and what you can do next
Other Keywords	
QUIT	Gets back to the previous level in the keyword hierarchy or terminates the run
COMMENT	Allows the user to annotate a run in a log file
STATUS	Gives the status of the mode keywords and the names of the fuel model file and the log file

Figure 2—Keyword summary for the BURN subsystem (FIRE1 and FIRE2 programs).



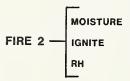


Figure 3—Keyword hierarchy for the BURN subsystem (FIRE1 and FIRE2 programs).

SUMMARY OF ADDITIONS AND CHANGES

The following is a summary of the capabilities that have been added to BEHAVE. They are listed according to keyword. The remainder of this paper describes these items in detail.

LOG/NOLOG - When the LOG mode is set, the results of LIST, RUN, COMMENT, and CUSTOM are written to a file. When the NOLOG mode is set, nothing is written to the file.

COMMENT - The user is allowed to enter a description of the run.

ENGLISH/METRIC - The option of either English or metric units can be set.

PERCENT/DEGREES - The option of specifying slope as either percentage or degrees can be set.

STATUS - The status is given for the mode keywords and, if they are in use, the names of the fuel model file and the log file.

SCORCH - Crown scorch height can be calculated.

MORTALITY - Level of tree mortality can be calculated.

SPOT - The wind-driven surface fire option has been added. Several southern tree species have been added to the torching tree option.

MAP - Calculated distances can be translated to map measurements.

SLOPE - Slope can be calculated from topographic map measurements.

IGNITE - Probability of ignition can be calculated.

MOISTURE - Table and graphic options are available for the fine dead (1-hour) fuel moisture model that is also in SITE.

RH - Relative humidity can be calculated from wet bulb and dry bulb temperatures.

UTILITY KEYWORDS (LOG, NOLOG, COMMENT, ENGLISH, METRIC, PERCENT, DEGREES, STATUS)

Several new utility keywords are available in the FIRE1 and FIRE2 programs: LOG, NOLOG, COMMENT, ENGLISH, METRIC, PERCENT, DEGREES, and STATUS. Use of these keywords is illustrated in appendix A.

Saving Results in a File for Printing (LOG and NOLOG)

BEHAVE involves a lot of interaction between you and the computer. Although it is most convenient to access BEHAVE through a video display terminal, there is often a need to save results on paper. The input and output are needed, but not all of the questions and answers.

LOG and NOLOG are mode keywords. When the LOG mode is set, the results of LIST, RUN, COMMENT, and CUSTOM are saved in a file that can later be printed. You can turn the option on and off at any time by typing LOG or NOLOG. You should get in the habit of always typing LIST before RUN. Predictions are meaningful only if they are associated with their input values.

When you first type the keyword LOG, you are asked to specify a file name. When you are finished running the program, you will be reminded that you have logged some information to a file and that you should print that file immediately and then delete it. It is important that you follow this advice to avoid wasting disk space on unneeded files.

Programs are written in standard Fortran so that they can easily be transported to a variety of computers. File handling, however, is not standard among computers. Naming of files, as well as procedures for printing and deleting them, depends on the computer being used, not on the BEHAVE system.

Adding User Comments to Output (COMMENT)

The keyword COMMENT allows you to document your logged runs. After you enter the keyword COMMENT, you may type in as many lines of description as you wish. Up to 80 characters may be typed per line; each line must be followed by a return. Two asterisks typed on a line by themselves, followed by a return, indicate that you are finished with your comment.

Changing Units (ENGLISH, METRIC, PERCENT, and DEGREES)

The previous version of BEHAVE used only English units of measurement. You now have a choice of either English or metric. The units mode can be changed at any time by typing the keywords ENGLISH or METRIC. The default is ENGLISH. It is possible, for example, to enter input in English units, enter the keyword METRIC, and then obtain the output in metric units. An example of this is given in appendix A.

Both English and metric units are given on the input/ output sheets in appendix B. We have used the metric units that are acceptable to many fire specialists. Those who wish to permanently change the units used in their program may contact the authors. We will tell you where to change the source code.

You can specify slope steepness in either percentage or degrees whether you are using English or metric units. The mode can be changed at any time, using the keywords PERCENT or DEGREES. The default is PERCENT.

Checking the Status of Files and of Mode Keywords (STATUS)

The keyword STATUS allows you to check the status of the mode keywords and to see the names of the fuel model file and the log file that you are using. An example is shown in figure 4. Other examples are given in appendix A.

**** FIRE1 STATUS REQUEST ****

PROMPT MODE : WORDY DISPLAY MODE : PAUSE LOG FILE NAME : LOGFILE LOG FUNCTION : ON

FUEL FILE NAME: UNDECLARED DISPLAY UNITS: ENGLISH

SLOPE UNITS : PERCENT

Figure 4-Use of the keyword STATUS gives the current status of each of the mode keywords.

CROWN SCORCH HEIGHT (SCORCH)

The SCORCH module of the FIRE1 program predicts lethal crown scorch height from flame length, ambient temperature, and midflame windspeed. As can be seen in figure 3, SCORCH can be used as either an independent module or it can be linked to DIRECT. Predictions from SCORCH can also be carried over to the MORTALITY module, as described in the next section.

The model developed by Van Wagner (1973) estimates the maximum height in the convection column at which the lethal temperature for live crown foliage is reached. This temperature is assumed to be 140 °F (60 °C). The scorch height model is based on the relationship of fireline intensity to temperature above the fire and on the shape of the convection column as it is affected by light winds. Flame length is used as a measure of the intensity of the heat source. The model is based on 13 test fires: eight in a stand of red pine and white pine, two in jack pine, one in red oak, and two in a red pine plantation.

Figure 5 shows the results of using SCORCH as an independent module. In this case a range of flame lengths and midflame windspeeds are examined. Notice that for a fixed flame length of 4 feet, as windspeed increases, scorch height decreases. This is caused by the flattening effect of wind as illustrated in figure 6. Although two fires may each have flame lengths of 4 feet, scorch heights will differ if the windspeeds are different.

Figure 7 shows the results of SCORCH being linked to DIRECT. On a single fire, when the windspeed increases, the flame length also increases. This effect can be seen in figure 7A where flame length is calculated for a range of windspeeds. If flame length remains constant with increasing windspeed (as in figure 5), then it must have been balanced by a change in another variable, such as increasing fuel moisture. Notice that, for this example, three combinations of 1-hour fuel moisture and windspeed result in 4-foot flame lengths. The resulting scorch height predictions are circled in figure 7B. Notice where those three values appear on the table in figure 5.

When SCORCH is used independently, flame length is an input value. When SCORCH is linked to DIRECT (fig. 3), flame length is calculated. SCORCH can be linked to DIRECT when the steady-state assumptions (Part 1, p. 9) are appropriate. SCORCH can be used independently when the flame length is controlled by the pattern of ignition.

Effective windspeed is used in the calculation of flame length in DIRECT (Part 1, p. 16). Midflame windspeed is used in the scorch height calculation in SCORCH. The DIRECT run in figure 8A illustrates that the effective windspeed for flanking and backing fires (spread directions 90 and 180 degrees) is much less than for the head fire (spread direction 0 degrees). Midflame windspeed and calculated flame lengths in figure 8B are carried over for the scorch height calculations shown in figure 8C. For the head fire, the increasing flame lengths easily offset the flattening effect of wind, and scorch height increases. But the low flame lengths for the flanking and backing fires are tilted enough by the midflame wind that the scorch height decreases.

SCORCH							
1AMBIENT AIR TEMP, F	75.0						
2FLAME LENGTH, FT	1.0	2.0	3.0	4.0	5.0	6.0	7.0
3MIDFLAME WINDSPEED, MI/H	.0	1.0	2.0	3.0	4.0	5.0	6.0

					- 					
CROW	N SCORCH	HEIGH	IT, FT						(V4.0))
	LAME ENGTH	I I	MID	FLAME W	INDSPEE	D, MI/H				-
	(FT)	I I	0.	1.	2.	3.	4.	5.	6.	_
	1.	I I	3.	3.	2.	1.	1.	1.	0.	
	2.	I I	8.	8.	7.	6.	5.	3.	3.	
	3.	I I	15.	15.	14.	13.	11.	9.	7.	
١	4.	I	23.	23.	22.	21.	18.	16.	14.	
L	5.	I	32.	32.	31.	30.	27.	25.	22.	
	6.	I	41.	41.	41.	40.	37.	34.	31.	
	7.	I I	52.	52.	51.	50.	48.	45.	42.	
	1 .	-	, 2	,	J	,				

Figure 5—Example independent SCORCH run. Note that for a fixed flame length, as windspeed increases, crown scorch height decreases.

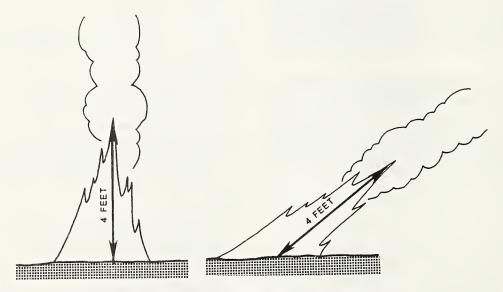


Figure 6—A 4-foot flame with no wind results in higher crown scorch height than a 4-foot flame which is flattened by the wind.

```
2 -- TIMBER (GRASS AND UNDERSTORY)
   1--FUEL MODEL
                           4.0 6.0 8.0 10.0 12.0
   2--1-HR FUEL MOISTURE, %
   3--10-HR FUEL MOISTURE, %
                            6.0
   4--100-HR FUEL MOISTURE, %
                            6.0
                          200.0
   5--LIVE HERBACEOUS MOIS, %
                                          3.0
                                               4.0
                                                    5.0
                                                         6.0
   7--MIDFLAME WINDSPEED, MI/H
                                1.0
                                      2.0
                             .0
                             .0
   8--TERRAIN SLOPE, %
   9--DIRECTION OF WIND VECTOR
                             .0
  10--DIRECTION OF SPREAD
                             .O (DIRECTION OF MAX SPREAD)
     CALCULATIONS
      DEGREES CLOCKWISE
       FROM THE WIND VECTOR
  ______
                                                 (V4.0)
A FLAME LENGTH, FT
  ______
              MIDFLAME WIND, MI/H
    1-HR
         Ι
    MOIS
         Ι
                                     4.
                                                6.
         Ι
              0.
                 1.
                        2.
                               3.
                                          5.
    (%)
         I-----
         Ι
                              4.0
    4.
          Ι
                         3.0
                                    5.0
                                          5.9
                                               6.8
              1.7
                   2.2
                                               6.2
                                    4.5
                                          5.4
    6.
          Ι
              1.5
                   2.0
                         2.8
          Ι
    8.
              1.4
                                    4.3
                                          5.1
                                               5.9
          Ι
                   1.9
                         2.7
                              3.5
          Ι
                                    4.0
                                          4.7
                                               5.5
   10.
          Ι
              1.3
                   1.7
                         2.5
                               3.2
          Ι
                                                4.6
   12.
              1.1
                   1.4
                         2.0
                               2.7
                                    3.3
  SCORCH-LINKED-TO-DIRECT
   1--AMBIENT AIR TEMP. F
                           75.0
                           OUTPUT FROM DIRECT. RANGE =
                                                    1.1 TO
                                                            6.8
   2--FLAME LENGTH, FT
   3--MIDFLAME WINDSPEED, MI/H SAVED FROM DIRECT. RANGE =
                                                    .O TO
                                                             6.0
   (V4.0)
  CROWN SCORCH HEIGHT, FT
   ______
      1-HR
             I
                 MIDFLAME WIND, MI/H
             Ι
      MOIS
                  0.
                                        4.
             I
                             2.
                                   3.
                                            5.
                                                    6.
                        1.
      (%)
             I-----
      4.
                                  21.
                                        27.
                                             33.
                                                   39.
                  6.
                       9.
                            15.
             Ι
             Ι
                                                   34.
      6.
             Ι
                  6.
                       8.
                            13.
                                  18.
                                        23.
                                             28.
             Ι
                                             26.
                                                   30.
                       8.
                                  16.
                                        21.
       8.
             Ι
                            12.
                  5.
             Ι
```

DIRECT

10.

12.

Ι

Ι

Ι

5.

4.

Figure 7—SCORCH linked to DIRECT. Three combinations of 1-hour moisture and windspeed give predicted flame lengths of 4 feet as indicated in 7A. The corresponding scorch height predictions are given in 7B.

7.

5.

10.

8.

14.

10.

18.

13.

22.

16.

26.

18.

```
1--FUEL MODEL
     7 - 2--1-HR FUEL MOISTURE, % 10.0 3--10-HR FUEL MOISTURE, % 10.0 4--100-HR FUEL MOISTURE
                          7 -- SOUTHERN ROUGH
     4--100-HR FUEL MOISTURE, % 10.0
6--LIVE WOODY MOISTURE, % 150.0
     7--MIDFLAME WINDSPEED, MI/H
8--TERRAIN SLOPE, %
9--DIRECTION OF WIND VECTOR
10--DIRECTION OF SPREAD
.0 90.0 180.0
       CALCULATIONS
        DEGREES CLOCKWISE
         FROM THE WIND VECTOR
   A EFFECTIVE WINDSPEED, MI/H (V4.0)
     _____
     MIDFLAME I SPREAD DIRECTION, DEG
      WIND I
           I
              0. 90. 180.
      (MI/H) I-----
           T
           I
      0.
              .0 .0 .0
      2.
          I 2.0 .4
                        .0
           Т
      4.
             4.0 .6
                       .1
           Ι
                   .6
          I
              6.0
      6.
                        .1
     ______
   B FLAME LENGTH, FT
     ______
     MIDFLAME I SPREAD DIRECTION, DEG
      WIND I I O. 90. 180.
      (MI/H) I-----
           Т
      0.
           I 1.2 1.2 1.2
           Ι
           I 2.8 1.5 1.2
      2.
           I
      4.
          I 4.1 1.6 1.2
           Ι
      6.
           I 5.3 1.7 1.2
SCORCH-LINKED-TO-DIRECT
 1--AMBIENT AIR TEMP, F 80.0
2--FLAME LENGTH, FT OUTPUT FROM DIRECT. RANGE = 1.2 TO 5.3
3--MIDFLAME WINDSPEED, MI/H SAVED FROM DIRECT. RANGE = .0 TO 6.0
CROWN SCORCH HEIGHT, FT
------
  MIDFLAME I SPREAD DIRECTION, DEG
   WIND
        I
         I 0. 90. 180.
  (MI/H)
        I-----
         Ι
    0.
         I
            4.
                 4. 4.
         T
    2.
        I 14.
                 5. 3.
        I
    4.
        I
            21.
                 3. 2.
            26.
         T
                 2.
                      1.
```

DIRECT

Figure 8—SCORCH linked to DIRECT. SCORCH uses midflame windspeed rather than effective windspeed.

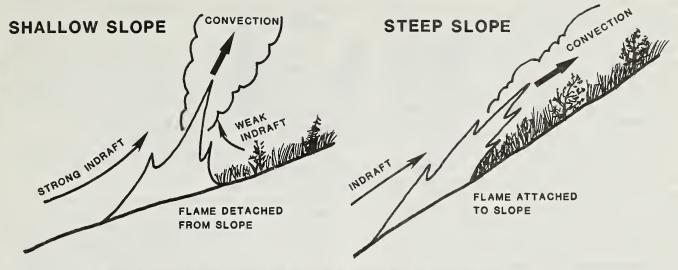


Figure 9—Flame detached from a shallow slope and flames attached to a steep slope.

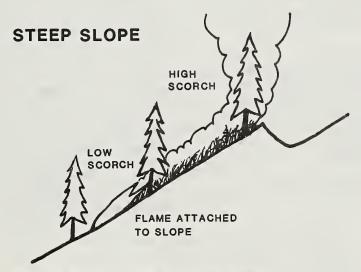


Figure 10—Scorching conditions on a steep slope.

The scorch height model was developed for flat ground. It should be used on slopes only with care. As pointed out in the previous example, the scorch height calculations use midflame windspeed, not effective windspeed. If SCORCH is used when percentage of slope is greater than zero, the slope is essentially ignored except in the effect that it has on the flame length calculations in DIRECT. SCORCH uses midflame windspeed as if the fire were on flat ground.

When using scorch height predictions in mountainous terrain, one must realize that the flame may or may not attach itself to the slope. When it does attach, the hot convective gases and smoke flow up the slope close to the surface rather than rising vertically as shown in figure 9. As stated by Rothermel (1985): "If an overstory of trees is present, the scorch height of trees on a steep slope will be affected. Attachment of the flame to the slope will reduce

the scorch height in trees above the flames from what would be expected on level ground where the flames stand vertically. But further up the slope at a ridge line where the convection column breaks from the surface and rises, the concentration of hot gases will scorch higher than expected on the flat." (See fig. 10.) Rothermel further points out that there is no definitive research on the problem of flame attachment. It appears from both lab work and discussions with users that the flame becomes attached near 50 percent slope when there is no prevailing wind.

Care should be taken in applying the scorch height predictions outside of the range of conditions for the 13 test fires used in developing the model. Fireline intensities for those fires were from 19 to 363 Btu/ft/s, which according to the equations used in BEHAVE, convert to flame lengths of 1.8 to 6.8 feet. The scorch heights were

from 6.5 to 56 feet. Temperatures were 73 to 88 °F and midflame windspeeds were 1.5 to 3 mi/h. According to Van Wagner (1973): "Since scorch height for the present set of fires is so well correlated with fire intensity alone, there is not much room for improvement by adding the effects of air temperature and wind.... If air temperature or wind differ markedly from average, then their additional effects may be tentatively estimated from the theory presented."

Other limitations of SCORCH are related to the model that is used to calculate flame length in DIRECT. In developing the crown scorch model, Van Wagner calculated fireline intensity from measurements of rate of spread and of fuel weight before and after burning. In BEHAVE, we use calculated flame length and fireline intensity as described on p. 10-11 of Part 1. This calculation is weighted to the fine fuels and does not include larger fuels that burn after the flaming front has passed. An alternative to using calculated flame length is to use SCORCH independent of DIRECT and enter flame length directly.

The models in DIRECT also assume that fuels are uniform and continuous. SCORCH then gives average values over an area, although variation within a single fire may be considerable.

As with all mathematical models that are used for fire behavior prediction, the scorch height model has limitiations. Even though fire managers are aware of those limitations, they use it frequently in prescribed fire planning. SCORCH was added to BEHAVE because of overwhelming user request. The appeal is that it is a simple model with few inputs. It gives a quantitative link between fire behavior and fire effects.

TREE MORTALITY LEVEL (MORTALITY)

The MORTALITY module of the FIRE1 program predicts percentage of tree mortality from scorch height, tree height, crown ratio, and bark thickness (which can be determined from tree species and tree diameter). It can be used in designing fire prescriptions that achieve acceptable tree survival. As shown in figure 3, MORTALITY can be used as an independent module. It can also be linked to SCORCH, which in turn can either be used independently or linked to DIRECT as described in the previous section.

The model was developed by Ryan and Reinhardt (1988). Formulation for managers including a nomogram and discussion of applications is given in Reinhardt and Ryan (1988). The model is based on tree mortality data taken on 43 prescribed fires in four Western States. This included 2,356 individual trees and seven western conifer species. Mortality was monitored for at least 2 years following the fire.

The model is based on the assumption that trees of different species are similar in their response to a given level of injury and that the level of damage depends on the fire and on tree characteristics (bark thickness, tree height, crown ratio). The basic model in MORTALITY calculates percentage of mortality from bark thickness and percentage of crown volume scorched. In order to make the model more useful as a predictive tool, bark thickness can be either entered directly or determined by tree diameter and species, and percentage of crown volume scorched is calculated from scorch height, tree height, and crown ratio. The relationship among the input values, intermediate values, and percentage of mortality is shown in figure 11. An illustration of several crown ratio values is shown in figure 12.

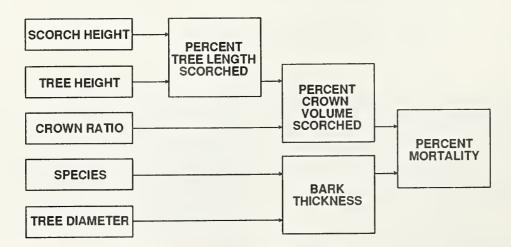


Figure 11—MORTALITY module user input, intermediate values, and final result.

CROWN RATIO



Figure 12—Illustration of three crown ratio values. Crown ratio is an input to MORTALITY.

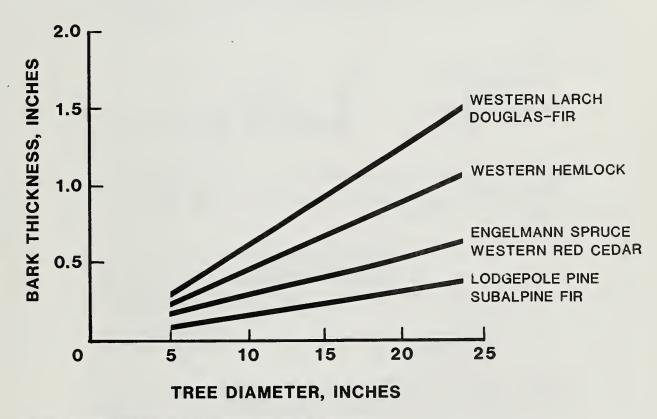


Figure 13—Bark thickness is estimated from tree diameter and species.

The model assumes that the amount of cambium damage is dependent on bark thickness. Bark thickness-tree diameter relationships for the species included in the study are given in figure 13. Only these are included in MORTALITY because the model has not yet been tested on other species. But with this in mind, you can choose the species with the bark thickness relationship that best fits the species you are concerned with or you can enter bark thickness directly.

Mortality predictions can be applied either to a stand or to an individual tree. A prediction of 30 percent mortality means that if 100 similar trees are subjected to the same fire, 30 of them are expected to die. Each tree either lives or dies. There is a 30 percent probability that an individual tree will die.

The basic assumptions of the model must be kept in mind when applying predictions of mortality to a specific area. "The model has an underlying assumption of a fire of average duration. Fires of very long duration will kill cambium through even the thickest bark, and will result in higher than predicted mortality. Thick layers of dry duff may result in long periods of smoldering even after the fire has moved through the area. Heavy concentrations of logs near trees will also result in extended duration of burning and a corresponding underprediction of mortality" (Reinhardt and Ryan 1988). On the other hand, mortality may be overpredicted if fuel is very light or patchy.

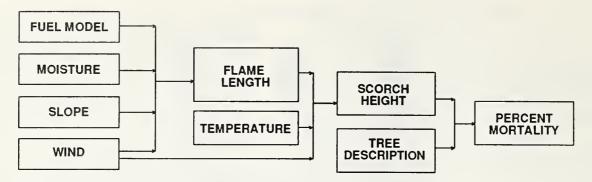


Figure 14—Information flow in MORTALITY linked to DIRECT and SCORCH. When SCORCH is linked to MORTALITY, flame length is input rather than calculated. When MORTALITY is used as an independent module, scorch height is input rather than calculated.

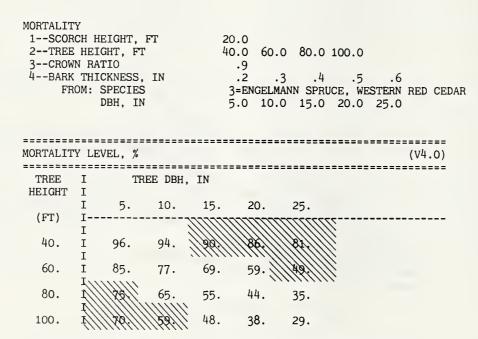


Figure 15—Independent MORTALITY run. A range of values is used for tree heights and diameters; scorch height is set to a constant value. Unrealistic combinations of tree height and diameter have been crossed off.

The MORTALITY module can be used in three ways: independent, linked to SCORCH, or linked to DIRECT and SCORCH as shown in figure 3. The choice depends on the application and on available information. Scorch height can be either entered directly (MORTALITY independent) or calculated by SCORCH. Flame length can be either entered directly (SCORCH-MORTALITY link) or calculated by DIRECT (DIRECT-SCORCH-MORTALITY link).

DIRECT-SCORCH-MORTALITY link information is shown in figure 14. DIRECT calculates flame length from fuel model, moisture, wind, and slope. SCORCH uses flame length and wind from DIRECT and ambient temperature to calculate crown scorch height. MORTALITY then uses scorch height and a description of the tree to calculate mortality. This option can be used if a prediction of the level of mortality is based on predicted fire behavior. The assumptions of the models in DIRECT and SCORCH must be met, most notably the steady-state assumption for the flame length calculation (Part 1, p. 9). If flame length is controlled by the pattern of ignition or if flame length is observed, then the SCORCH-MORTALITY link option can be used, allowing you to input flame length directly. If conditions violate the assumptions of the scorch height model (for example steep slopes), or if observed scorch height is available, then MORTALITY can be used as an independent module.

A run of MORTALITY as an independent module is shown in figure 15. This example is for a range of tree heights and tree diameters. Scorch height and crown ratio are held constant. Mortality level ranges from 29 to 96 percent. Some of the combinations of tree heights and diameters are unrealistic. Rather than setting arbitrary cutoff values, we let you make the decision and cross off values as we have done in figure 15.

Figure 16 gives an example of MORTALITY linked to SCORCH. Scorch height is calculated for a range of flame lengths. Mortality level is then calculated for trees of a specified height, crown ratio, species, and diameter.

Figure 17 is an example of the complete DIRECT-SCORCH-MORTALITY link. In this case, flame length is calculated for a range of windspeeds. SCORCH gives the corresponding scorch height values, and MORTALITY gives percentage of mortality expected under these conditions.

SCORCH

```
1--AMBIENT AIR TEMP, F ---- 80.0
2--FLAME LENGTH, FT ----- 2.0 4.0 6.0 8.0 10.0
3--MIDFLAME WINDSPEED, MI/H 2.0
```

- (V	4.0)	
FLAME	Ι	CROWN
LENGTH	Ι	SCORCH
	I	HEIGHT
(FT)	I	(FT)
	Ι	
2.0	I	8.
	I	
4.0	I	24.
	I	
6.0	Ι	44.
	Ι	
8.0	Ι	67.
	I	
10.0	I	94.

MORTALITY-LINKED-TO-SCORCH

1SCORCH HEIGHT, FT 2TREE HEIGHT, FT 3CROWN RATIO	OUTPUT FROM SCORCH. RANGE = 80.0 .8	8. TO	94.
4BARK THICKNESS, IN FROM: SPECIES DBH, IN	1.3 1=WESTERN LARCH, DOUGLAS-FIR 20.0		

(V	4.0)		
FLAME	I	MORTALITY	CROWN
LENGTH	Ι	LEVEL	VOLUME
	I		SCORCH
(FT)	Ι	(%)	(%)
	I		
2.0	Ι	5.	0.
	Ι		
4.0	Ι	7.	24.
	Ι		
6.0	Ι	41.	69.
	Ι		
8.0	Ι	89.	96.
	Ι		
10.0	Ι	92.	100.

Figure 16—MORTALITY linked to SCORCH. A range of flame lengths is input into SCORCH.

```
DIRECT
 1--FUEL MODEL
                                 2 -- TIMBER (GRASS AND UNDERSTORY)
                                4.0
 2--1-HR FUEL MOISTURE, %
 3--10-HR FUEL MOISTURE, %
                                 6.0
 4--100-HR FUEL MOISTURE, %
                                 6.0
 5--LIVE HERBACEOUS MOIS, %
                               200.0
 7--MIDFLAME WINDSPEED, MI/H
                                 3.0
                                       4.0
                                             5.0
 8--TERRAIN SLOPE, %
                                  .0
 9--DIRECTION OF WIND VECTOR
                                  .0
10--DIRECTION OF SPREAD
                                  .0
                                      (DIRECTION OF MAX SPREAD)
    CALCULATIONS
     DEGREES CLOCKWISE
      FROM THE WIND VECTOR
      (V4.0)
MIDFLAME I RATE OF HEAT PER
                               FIRELINE FLAME
                                                  REACTION EFFECT.
        I SPREAD UNIT AREA INTENSITY LENGTH INTENSITY WIND
 (MI/H)
        I (CH/H) (BTU/SQFT) (BTU/FT/S) (FT) (BTU/SQFT/M) (MI/H)
         Ι
   3.
         Ι
             13.
                      492.
                                  116.
                                           4.0
                                                   3567.
                                                               3.0
         Ι
   4.
                      492.
                                  184.
                                                               4.0
         Ι
             20.
                                                   3567.
                                           5.0
         Ι
         Ι
             30.
                      492.
                                  268.
                                                   3567.
                                                               5.0
   5.
                                           5.9
SCORCH-LINKED-TO-DIRECT
 1--AMBIENT AIR TEMP, F
                                75.0
                                                               4.0 TO
                                OUTPUT FROM DIRECT. RANGE =
 2--FLAME LENGTH, FT
                                                                          5.9
                               SAVED FROM DIRECT. RANGE =
                                                               3.0 TO
 3--MIDFLAME WINDSPEED, MI/H
                                                                          5.0
               (V4.0)
         MIDFLAME I
                       CROWN
           WIND
                      SCORCH
                  Ι
                      HEIGHT
                  Ι
          (MI/H)
                  Ι
                        (FT)
                  Ι
                  Ι
                         21.
          3.
                  Ι
          4.
                  Ι
                         27.
                  Ι
          5.
                  Τ
                         33.
MORTALITY-LINKED-TO-DIRECT-AND-SCORCH
                                 OUTPUT FROM SCORCH. RANGE = 21. TO
                                                                        33.
 1--SCORCH HEIGHT, FT
                                50.0
 2--TREE HEIGHT, FT
                                 .5
 3--CROWN RATIO
 4--BARK THICKNESS, IN
                                  .1
                                 4=LODGEPOLE PINE, SUBALPINE FIR
      FROM: SPECIES
            DBH, IN
                                10.0
      (V4.0)
                              CROWN
MIDFLAME I
             MORTALITY
                              VOLUME
  WIND
         Ι
                LEVEL
                              SCORCH
         Ι
  (MI/H)
                 (%)
                                (%)
         Ι
                  68.
                                  0.
    3.
         Ι
         Ι
    4.
         Ι
                  71.
                                 15.
          Ι
                  92.
                                 55.
    5.
         Ι
```

Figure 17—MORTALITY linked to DIRECT and SCORCH. Flame length is calculated for a range of windspeeds in DIRECT.

MAXIMUM SPOTTING DISTANCE FROM WIND-DRIVEN SURFACE FIRES (SPOT)

The SPOT module of the FIRE1 program predicts the maximum distance that a firebrand will travel from torching trees, a burning pile of debris, or from a wind-driven surface fire. Use of SPOT for torching trees and burning piles is described in Part 1 (p. 47-49). The only change to those options is that additional tree species have been added to the torching tree option: slash pine, longleaf pine, pond pine, shortleaf pine, and loblolly pine (Albini 1979). The option of spotting from wind-driven surface fires (Albini 1983; Chase 1984; Morris 1987) has been added and is described here.

The option of spotting from a wind-driven surface fire can be either an independent SPOT run or linked with DIRECT. Input requirements are flame length, wind-speed, and a description of the terrain. In a linked run, flame length and windspeed, are carried over from DIRECT to SPOT.

The basic assumptions that apply to all options of the spotting model are repeated here. The model is designed to predict intermediate-range spotting, not short-range spotting such as debris blowing just across a fire line. We are concerned with spots that occur far enough from the main fire to grow as independent fires. But we are not dealing with the problem of very extreme fire behavior conditions, where spotting is caused by large firebrands (even logs) being carried into the combustion column. Predictions are for maximum spotting distance because ideal conditions are assumed. Firebrands are assumed to be sufficiently small to be carried some distance, yet large enough to still be able to start a fire when they reach the ground. The model, however, does not address the problem of firebrands such as eucalyptus bark that literally fly through the air.

The process by which firebrands are transported from wind-driven surface fires is postulated to be that of lofting of particles by line thermals that are generated by variations in the intensity of the fire. The model is based on the assumption that the fire front is approximated by a straight line perpendicular to the direction of the wind. Predictions therefore apply to wind-driven head fires, not flanking or backing fires and not fires whose spread is influenced more by the slope than by the wind.

Use of the predictions of spotting distance from winddriven surface fires is restricted to cases where there is no overstory. Mean cover height is set to zero. Fires burning under standing timber seldom cause spot fires at any significant distance unless the trees of the overstory become involved in the fire. The overstory is a barrier that intercepts firebrands and also interferes with development of a strong updraft that can lift firebrand particles. Some fuel models ordinarily have overstories, but are sometimes used to represent fuels without overstory cover. For example, fuel model 10 (timber litter and understory) is sometimes used to represent timber harvest debris overgrown with shrubs or other vegetation.

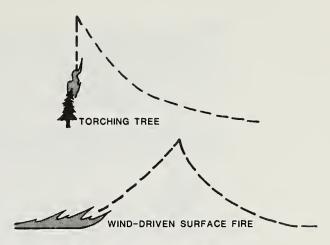


Figure 18—A firebrand from a torching tree or a burning pile is lifted straight up and then carried by the prevailing wind. This is compared to a firebrand from a wind-driven surface fire, which is carried some distance downwind from the firefront where the thermal originated before it is carried by the prevailing wind.

All three spotting source location options use the same method of calculating the distance that a firebrand is carried by the prevailing wind. The difference is in calculating initial lofting height. For the torching tree option, a description of the trees is used to calculate transitory flame characteristics. For the burning pile option, continuous flame height is entered directly. For the wind-driven surface fire option, flame length is used as an indicator of the energy in a thermal from a line fire. When the particle exits the rising thermal, it will be some distance downwind from the firefront where the thermal originated. Figure 18 illustrates the difference in the trajectories of a firebrand from a torching tree and from a wind-driven surface fire.

SPOT is offered both independently and linked to DIRECT as shown in figure 3. The independent option is included to allow the flexibility of examining the spotting distance model on its own. You are allowed to enter any value for the required input as done in figures 19 and 20 described below. But the most common use of the wind-driven surface fire option of SPOT will probably be linked to DIRECT, which calculates flame lengths, as shown in figures 21 and 22. Because flame length is not used in the torching tree or burning pile options, only the wind-driven surface fire option can be linked to DIRECT.

Figure 19 shows independent SPOT runs for two spotting source options: burning pile and wind-driven surface fire. In both cases, the mean cover height is zero. The same range of windspeeds was used in each case. And the same values were used for continuous flame height and for flame length. Notice that the predicted spotting distances are longer for the wind-driven surface fire option. This example is used to point out the difference in continuous flame height from a burning pile of debris and the flame length from a wind-driven surface fire. It also illustrates the effect of the difference in lofting mechanisms.

SPOT										
1FIREBRAN	ND SOL	JRCE		2BI	JRNING	PILE	7			
2MEAN CO	VER HE	EIGHT, F	[.0			_			
320-F00T 4RIDGE/V	WINDS ALLEY	SPEED, MI ELEVATIO	I/H ON	5.0	10.0	15.0	20.0	25.0	30.0	35.0
•		RENCE, FI		.0						
11CONTINUO	OUS FI	LAME HT,	FT	4.0	8.0	12.0	16.0	20.0	24.0	28.0
=========				====:	======	=====				
MAXIMUM SPO			•						(V4.0)	
=========								=====		
20-FT	I	CON	rinuous	FLAMI	r ueign	I, FI				
WINDSPEED	Ī	4.	8.	12.	16	20	. 2	ь	28	
(MI/H)								.T.		
(/	Ī									
5.	I	.0	.1	.1	.1		. 1	.1	.1	
	I						. –	• -		
10.	I	.1	.1	.1	.2		.2	.2	.2	
	I						_	-		
15.	I	.1	.2	.2	.2		. 3	.3	.3	
	I									
20.	I	.1	.2	٠3	.3		. 4	. 4	.5	
	I	. –	• -					• •		
25.	Ī	.2	.3	. 3	. 4		.5	•5	.6	
-2.	Ī		• 5	• 5	• '		•)	•)		
30.	Ī	.2	3	.4	5		.6	.6	.7	
50.	Ī	• -	• 5	• 4	•)		• 0	• 0	• 1	
35.	Ī	.2	lı	٠5	6		.7	.7	.8	
3).	-		• 7	•)	. 0		• 1	• 1	.0	
SDOT										
SPOT	IDS AIM	IDCE		3 M.	IND_DDT	VEN CI	IDEACE	FIDE	1	
1FIREBRAI	ND SOL	JRCE			IND-DRI	VEN SI	URFACE	FIRE]	
1FIREBRAI 2MEAN CO	VER HE	EIGHT, FI	ľ	.0						25 0
1FIREBRAN 2MEAN CO 320-FOOT	VER HE WINDS	EIGHT, FI SPEED, MI	Г Г/Н	.0						35.0
1FIREBRAI 2MEAN COV 320-FOOT 4RIDGE/VA	VER HE WINDS ALLEY	EIGHT, F1 SPEED, M1 ELEVATIO	r L/H DN	.0 5.0						35.0
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/VA	VER HE WINDS ALLEY DIFFEF	EIGHT, FI SPEED, MI ELEVATION RENCE, FI	C L/H DN C	.0 5.0	10.0	15.0	20.0	25.0	30.0	
1FIREBRAI 2MEAN COV 320-FOOT 4RIDGE/VA	VER HE WINDS ALLEY DIFFEF	EIGHT, FI SPEED, MI ELEVATION RENCE, FI	C L/H DN C	.0 5.0	10.0	15.0	20.0	25.0		
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/VA	VER HE WINDS ALLEY DIFFEF	EIGHT, FI SPEED, MI ELEVATION RENCE, FI	C L/H DN C	.0 5.0	10.0	15.0	20.0	25.0	30.0	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/VA	VER HE WINDS ALLEY DIFFEF ENGTH,	EIGHT, FT SPEED, MI ELEVATIO RENCE, FT	C L/H DN C	.0 5.0 .0 4.0	10.0	15.0 12.0	20.0	25.0	30.0	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V	VER HE WINDS ALLEY DIFFEF ENGTH,	EIGHT, FT SPEED, MI ELEVATIO RENCE, FT FT	r I/H DN r	.0 5.0 .0 4.0	8.0	15.0 12.0	20.0	25.0	30.0	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V	VER HE WINDS ALLEY DIFFEF ENGTH, =====	GIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE	f I/H DN f ======	.0 5.0 .0 4.0	8.0	15.0 12.0	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI MAXIMUM SPO	VER HE WINDS ALLEY DIFFEF ENGTH, =====	GIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE	C I/H DN C ======	.0 5.0 .0 4.0	8.0	15.0 12.0	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI MAXIMUM SPO	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING II	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI FT DISTANCE	C L/H DN C E, MI ===== ME LENG	.0 5.0 .0 4.0	8.0	15.0 12.0 =====	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING II	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI FT DISTANCE	C L/H DN C E, MI ===== ME LENG	.0 5.0 .0 4.0	8.0	15.0 12.0 =====	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING I I I	GIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE	TI/H DN T E, MI THE LENGT	.0 5.0 .0 4.0	8.0	15.0 12.0 =====	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING I I I I I	EIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE FLAM	TI/H DN T E, MI THE LENGT	.0 5.0 .0 4.0	8.0	15.0 12.0 =====	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI MAXIMUM SPO 20-FT WINDSPEED (MI/H)	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING ===== I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE FLAM	fi/H DN f E, MI ME LENG	.0 5.0 4.0	10.0	15.0 12.0 ===== 20	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING ===== I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE FLAM	TI/H DN T E, MI THE LENGT	.0 5.0 .0 4.0	10.0	15.0 12.0 ===== 20	20.0	25.0	30.0 24.0 (V4.0)	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ITING I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI FI DISTANCE FLAM	E LENG	.0 5.0 4.0 4.0	10.0 8.0 16.	15.0	20.0	25.0	30.0 24.0 (V4.0) 28.	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI MAXIMUM SPO 20-FT WINDSPEED (MI/H)	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING ====== I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATION RENCE, FI FT DISTANCE FLAM	fi/H DN f E, MI ME LENG	.0 5.0 4.0	10.0 8.0 16.	15.0	20.0	25.0	30.0 24.0 (V4.0) 28.	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI E	VER HE WINDS ALLEY DIFFEF ENGTH, I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI DISTANCE FLAM 4.	E, MI E, MI E, ME LENG 8.	.0 5.0 4.0 4.0 =====: TH, F.	10.0 8.0 16. .2 .4	15.0	20.0	25.0 20.0 20.0 24. .3	30.0 24.0 ====== (V4.0) ===== 28. .4 .6	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING I I I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI FI DISTANCE FLAM	E LENG	.0 5.0 4.0 4.0 	10.0 8.0 16.	15.0	20.0	25.0	30.0 24.0 (V4.0) 28.	
1FIREBRAI 2MEAN CO' 320-FOOT 4RIDGE/V 112FLAME LI ====================================	VER HE WINDS ALLEY DIFFEF ENGTH, ====== ITING I I I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI DISTANCE FLAM 41 .2	E., MI E. LENG 82 .2	.0 5.0 .0 4.0 =====: TH, F. 12. .2 .3	10.0 8.0 16. .2 .4	15.0	20.0	25.0 20.0 20.0 24. -3 .5	30.0 24.0 24.0 (V4.0) ===== 28. .4 .6	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI E	VER HE WINDS ALLEY DIFFEF ENGTH, I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI DISTANCE FLAM 4.	E, MI E, MI E, ME LENG 8.	.0 5.0 4.0 4.0 =====: TH, F.	10.0 8.0 16. .2 .4	15.0	20.0	25.0 20.0 20.0 24. .3	30.0 24.0 ====== (V4.0) ===== 28. .4 .6	
1FIREBRAI 2MEAN CO' 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, FITING FIT	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI DISTANCE FLAN 41 .2 .2 .2	E., MI E., ME LENG 82 .2 .3 .4	.0 5.0 4.0 =====: TH, F. 12. .2 .3 .4	10.0 8.0 16. .2 .4 .5	15.0 12.0 ===== 20	20.0 16.0 ====== . 2 .3 .5 .6	25.0 20.0 20.0 24. .3 .5 .7	30.0 24.0 ====== (v4.0) ===== 28. .4 .6 .8 .9	
1FIREBRAI 2MEAN CO' 320-FOOT 4RIDGE/V 112FLAME LI ====================================	VER HE WINDS ALLEY DIFFEF ENGTH, FITING FITING I I I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI DISTANCE FLAM 41 .2	E., MI E. LENG 82 .2	.0 5.0 4.0 =====: TH, F. 12. .2 .3 .4	10.0 8.0 16. .2 .4	15.0 12.0 ===== 20	20.0	25.0 20.0 20.0 24. -3 .5	30.0 24.0 24.0 (V4.0) ===== 28. .4 .6	
1FIREBRAI 2MEAN CO' 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ITING I I I I I I I I I I I I I I I I I I	EIGHT, FISPEED, MI ELEVATION RENCE, FI DISTANCE FLAM 4. .1 .2 .2 .2 .3	E, MI E, MI E, MI 8. .2 .2 .3 .4 .5	.0 5.0 .0 4.0 =====: ITH, F: 12. .3 .4 .5	10.0 8.0 16. .2 .4 .5 .6	15.0 12.0 ===== 20	20.0 16.0 . 2 .3 .5 .6 .7	25.0 20.0 20.0 24. .3 .5 .7 .8	30.0 24.0 (V4.0) 28. .4 .6 .8 .9 1.1	
1FIREBRAI 2MEAN CO' 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING I I I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATIO RENCE, FI DISTANCE FLAN 41 .2 .2 .2	E., MI E., ME LENG 82 .2 .3 .4	.0 5.0 .0 4.0 =====: ITH, F: 12. .3 .4 .5	10.0 8.0 16. .2 .4 .5 .6	15.0 12.0 ===== 20	20.0 16.0 ====== . 2 .3 .5 .6	25.0 20.0 20.0 24. .3 .5 .7	30.0 24.0 ====== (v4.0) ===== 28. .4 .6 .8 .9	
1FIREBRAI 2MEAN CO 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING I I I I I I I I I I I I I I I I I I	EIGHT, FI SPEED, MI ELEVATION RENCE, FI DISTANCE FLAM 41 .2 .2 .2 .3 .3	E, MI E, MI 82 .2 .3 .4 .5	.0 5.0 .0 4.0 ====: IH, F: 12. .3 .4 .5 .6	10.0 8.0 16. .2 .4 .5 .6 .7	15.0	20.0 16.0 . 2 .3 .5 .6 .7 .9	25.0 20.0 20.0 24. .3 .5 .7 .8 1.0	30.0 24.0 24.0 (V4.0) 28. .4 .6 .8 .9 1.1 1.2	
1FIREBRAI 2MEAN CO' 320-FOOT 4RIDGE/V 112FLAME LI	VER HE WINDS ALLEY DIFFEF ENGTH, ===== ITING I I I I I I I I I I I I I I I I I I	EIGHT, FISPEED, MI ELEVATION RENCE, FI DISTANCE FLAM 4. .1 .2 .2 .2 .3	E, MI E, MI E, MI 8. .2 .2 .3 .4 .5	.0 5.0 .0 4.0 =====: ITH, F: 12. .3 .4 .5	10.0 8.0 16. .2 .4 .5 .6 .7	15.0	20.0 16.0 . 2 .3 .5 .6 .7	25.0 20.0 20.0 24. .3 .5 .7 .8	30.0 24.0 (V4.0) 28. .4 .6 .8 .9 1.1	

Figure 19—Independent SPOT runs for two spotting source options: burning pile and wind-driven surface fire.

1	SPOT									
	1FIREBRAN				3WIN	D-DRIVEN	SURFACE	FIRE		
	2MEAN COV				.0				20.0	25.0
	320-FOOT 4RIDGE/VA				5.0 1	0.0 15.0	20.0	25.0	30.0	35.0
	I	DIFFER	RENCE, FT		0. 10	00. 2000.	3000.	4000.		
	5RIDGE/VA		HORIZONI ICE, MI	AL	1.0					
	6SPOTTING	SOUF	CE LOCAT	CION		IDSLOPE,	WINDWAF	RD SIDE	1	
	12FLAME LI				20.0	····			_	
	MAXIMUM SPOT								(V4.0)	
	20-FT					ATIONAL D		ICE, FT		
	WINDSPEED			000.	2000. 3	3000. 400	00.			
	(MI/H)	I								
	、 5・		•3	.3	.3	.3	.4			
		I								
	10.	I	•5	•5	٠5	.6	٠7			
	15.	I	.6	. 7	.7	.8	.9			
	-)•	Ī	.0	• ,	• •		• /			
	20.	I	.7	.8	.9	.9	1.0			
	0.5	I	•		4.0					
	25.	I	.9	٠9	1.0	1.1	1.1			
	30.	I	1.0	1.0	1.1	1.2	1.2			
	55.	Ī								
	35•	I	1.1	1.1	1.2	1.2	1.3			
_										
В	SPOT 1FIREBRA	MD SOI	IDCE		2WTI	ND-DRIVEN	SIIDEAC	e eree		
	2MEAN CO				.0	AD-DUTAEM	SUNFAC	E LIVE		
	320-F00T	WINDS	SPEED, M	I/H		10.0 15.0	20.0	25.0	30.0	35.0
	4RIDGE/V									
	5RIDGE/V		RENCE, F		0. 10	000. 2000	. 3000.	4000.		
			NCE, MI	IAL	1.0					
	6SPOTTIN			TION		MIDSLOPE,	LEEWAR	D SIDE	٦	
	12FLAME L	ENGTH	, FT		20.0				-	
	=========									
	MAXIMUM SPO								(V4.0)	
	========				======					
	20-FT	I				VATIONAL I		NCE, FI	1	
	WINDSPEED	I	0. 10	വവ	2000 1	2000 1100	20			
	/ n n = 1 - n \	_			2000.	3000. 400				
	(MI/H)					3000. 400				
		I								
	(MI/H) 5.				.3					
		I		.3		.3				
	5. 10.	I I I I	.3 .5	·3	·3	·3 .4	.3 .4			
	5.	I I I I I	.3	·3	.3	·3 .4	.3 .4			
	5. 10. 15.	I I I I I	.3 .5	.3 .4 .6	.3 .4 .5	.3 .4 .5	.3 .4 .5			
	5. 10.	I I I I I	.3 .5	.3 .4 .6	.3 .4 .5	.3 .4 .5 .6	.3 .4			
	5. 10. 15.	I I I I I I I I I I I I I I	.3 .5 .6	.3 .4 .6	.3 .4 .5	.3 .4 .5 .6	.3 .4 .5			
	5. 10. 15. 20. 25.		.3 .5 .6 .7	.3 .4 .6 .7	.3 .4 .5 .7	.3 .4 .5 .6	.3 .4 .5 .6			
	5. 10. 15. 20.		.3 .5 .6 .7	.3 .4 .6	.3 .4 .5	.3 .4 .5 .6	.3 .4 .5 .6			
	5. 10. 15. 20. 25.		.3 .5 .6 .7	.3 .4 .6 .7	.3 .4 .5 .7 .8	.3 .4 .5 .6 .7	.3 .4 .5 .6			

Figure 20—Independent SPOT run for two spotting source locations.

```
DIRECT
1--FUEL MODEL
                                6 -- DORMANT BRUSH, HARDWOOD SLASH
2--1-HR FUEL MOISTURE, %
                               8.0
 3--10-HR FUEL MOISTURE, %
                              10.0
4--100-HR FUEL MOISTURE, %
                              10.0
7--MIDFLAME WINDSPEED, MI/H
                               5.0 10.0 15.0 20.0 25.0
8--TERRAIN SLOPE, %
                                .0
9--DIRECTION OF WIND VECTOR
                                .0
10--DIRECTION OF SPREAD
                                .O (DIRECTION OF MAX SPREAD)
   CALCULATIONS
    DEGREES CLOCKWISE
     FROM THE WIND VECTOR
```

(V4	. (0)				i	
MIDFLAME	Ι	RATE OF	HEAT PER	FIRELINE	FLAME	REACTION	EFFECT.
WIND	Ι	OI IIIII	UNIT AREA	INTENSITY	LENGTH		WIND
(MI/H)	Ι	(CH/H)	(BTU/SQFT)	(BTU/FT/S)	(FT)	BTU/SQFT/M)	(MI/H)
	Ι						
5.	Ι	29.	436.	235.	5.5	1777.	5.0
	Ι						
10.	Ι	72.	436.	576.	8.4	1777.	10.0
	Ι			0 -			
15.	Ī	123.	436.	983.	10.7	1777.	15.0
	I		1.00				
20.	Ι	159.	436.	1268.	12.0	1777.	18.2*
	Ι		1 4	40			
25.	1	159.	436.	1268.	12.0	1777.	18.2*

^{*} MEANS YOU HIT THE WIND LIMIT.

SPOT-LINKED-TO-DIRECT							
1FIREBRAND SOURCE	3W	IND-DR	IVEN S	URFACE	FIRE		
2MEAN COVER HEIGHT, FT	.0						
320-FOOT WINDSPEED, MI/H	12.5	25.0	37.5	50.0	62.5		
FROM MIDFLAME WIND =	5.0	10.0	15.0	20.0	25.0		
& EXPOSED FUEL WAF =	. 4						
4RIDGE/VALLEY ELEVATION							
DIFFERENCE, FT	.0						
12FLAME LENGTH, FT	OUTP	UT FRO	M DIRE	CT. RAI	NGE=	5.5 TO	12.0

(V4.0)	
MIDFLAME	Ι	MAXIMUM
WIND	I	SPOTTING
	I	DISTANCE
(MI/H)	I	(MI)
	I	
5.	I	.2
	I	
10.	I	•5
	I	
15.	I	.7
	I	
20.	Ι	1.0
	Ι	
25.	I	1.1

Figure 21—SPOT linked to DIRECT. The maximum effective windspeed is used in the flame length calculations. The actual windspeed is used in the spotting distance calculations.

```
A DIRECT
   1--FUEL MODEL
                         4 -- CHAPARRAL, 6 FT (180 CM)
                      5.0 10.0 15.0
   2--1-HR FUEL MOISTURE, %
   3--10-HR FUEL MOISTURE, %
                        6.0
   4--100-HR FUEL MOISTURE, % 6--LIVE WOODY MOISTURE, %
                         6.0
                       150.0
   7--MIDFLAME WINDSPEED, MI/H 10.0 20.0 30.0
   8--TERRAIN SLOPE, %
                        20.0
   9--DIRECTION OF WIND VECTOR
      DEGREES CLOCKWISE
      FROM UPHILL
                     .O (DIRECTION OF MAX SPREAD)
  10--DIRECTION OF SPREAD
     CALCULATIONS
      DEGREES CLOCKWISE
      FROM UPHILL
  ------
  1-HR
        I MIDFLAME WIND, MI/H
   MOIS
        Ι
        I 10. 20. 30.
   (%)
        T-----
        Ι
        I 27.1 42.0 54.6
   5.
        I 24.4 37.8 49.1
   10.
        Ι
        I 11.2 17.5 22.7
   15.
  SPOT-LINKED-TO-DIRECT
                        3--WIND-DRIVEN SURFACE FIRE .0
   1--FIREBRAND SOURCE----
   2--MEAN COVER HEIGHT, FT
      FROM MIDFLAME WIND = 10.0 20.0 30.0 EXPOSED FUEL WAF = .6
   3--20-FOOT WINDSPEED, MI/H
   4--RIDGE/VALLEY ELEVATION
          DIFFERENCE, FT 1000.0
   5--RIDGE/VALLEY HORIZONTAL
          DISTANCE, MI
  6--SPOTTING SOURCE LOCATION O.-- MIDSLOPE, WINDWARD SIDE
  12--FLAME LENGTH, FT
                         OUTPUT FROM DIRECT. RANGE= 11.2 TO 54.6
  MAXIMUM SPOTTING DISTANCE, MI
  ______
          I MIDFLAME WIND, MI/H
     MOIS
          Ι
           I 10. 20. 30.
           I-----
     (%)
           Ι
              .9 1.8 2.8
           Ι
           Т
     10.
          I .8 1.7 2.6
           I
     15.
          I .5 1.0 1.5
```

Figure 22—SPOT linked to DIRECT. The direction of the wind vector is upslope in figure 22A and downslope in 22B.

```
B DIRECT
  1--FUEL MODEL
2--1-HR FUEL MOISTURE, % 5.0 10.0 15.0 3--10-HR FUEL MOISTURE, % 6.0
  1--FUEL MODEL
                           4 -- CHAPARRAL, 6 FT (180 CM)
  4--100-HR FUEL MOISTURE, % 6.0
6--LIVE WOODY MOISTURE, % 150.0
7--MIDFLAME WINDSPEED, MI/H 10.0 20.0 30.0
   8--TERRAIN SLOPE. %
                           20.0
  9--DIRECTION OF WIND VECTOR 180.0
      DEGREES CLOCKWISE
      FROM UPHILL
  10--DIRECTION OF SPREAD DIRECTION OF MAXIMUM SPREAD
     CALCULATIONS
                           TO BE CALCULATED
      DEGREES CLOCKWISE
      FROM UPHILL
  -----
  1-HR I MIDFLAME WIND, MI/H
       I
   MOIS
           10. 20.
         I
                       30.
   (%)
        I-----
                            ______
         Ι
   5.
       I
           26.5 41.7 54.4
  10.
        I 23.8 37.5 48.9
         Ι
  15. I 11.0 17.3 22.6
  SPOT-LINKED-TO-DIRECT
  1--FIREBRAND SOURCE------ 3--WIND-DRIVEN SURFACE FIRE 2--MEAN COVER HEIGHT, FT .0
  3--20-FOOT WINDSPEED, MI/H 16.7 33.3 50.0 FROM MIDFLAME WIND = 10.0 20.0 30.0 & EXPOSED FUEL WAF = .6
                          .6
  4--RIDGE/VALLEY ELEVATION
DIFFERENCE, FT 1000.0
  5--RIDGE/VALLEY HORIZONTAL
          DISTANCE, MI
  6--SPOTTING SOURCE LOCATION 2.-- MIDSLOPE, LEEWARD SIDE
  12--FLAME LENGTH, FT
                           OUTPUT FROM DIRECT. RANGE= 11.0 TO 54.4
  -----
  MAXIMUM SPOTTING DISTANCE, MI
  I MIDFLAME WIND, MI/H
     1-HR
     MOIS
              10. 20. 30.
           Ι
     (%)
           I-----
           Ι
           I .7 1.7 2.7
     5.
            Ι
                .7 1.6 2.5
     10.
            Ι
                .4 .9 1.5
     15.
           I
```

Figure 22 (Con.)

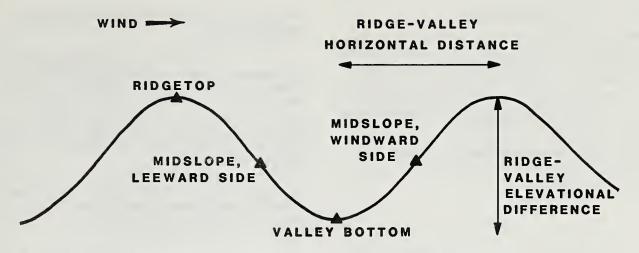


Figure 23—Mountainous terrain and spotting source location for the maximum spotting distance model.

Another use of SPOT as an independent module is to examine the effect of a change in the terrain description and spotting source location as shown in figure 20. Flame length is assigned a constant value of 20 feet. The spotting source location is midslope on the windward side for figure 20A and midslope on the leeward side for figure 20B. Recall that the spotting distance model defines the terrain with the smooth curve shown in figure 23.

Because predictions are for spotting from the head of a wind-driven fire, the link to DIRECT is allowed only when calculations are done for the direction of maximum spread as specified in line 10 input to DIRECT. In addition, spotting distance predictions are not given when the difference between the direction of the wind vector and the calculated direction of maximum spread is more than 30 degrees. In that case the fire no longer meets the assumptions of a wind-driven head fire. The direction of spread of the head fire is significantly different from the direction of the wind vector only for low windspeeds and steep slope.

The windspeed that is required by SPOT is the 20-foot windspeed while the windspeed input into DIRECT is at midflame height. The wind adjustment factor was designed to reduce 20-foot windspeed to midflame windspeed, and use in reverse is not recommended. But this is a no overstory situation and we are not concerned with slope winds. We therefore use the exposed-fuel wind adjustment factor associated with each fuel model (Part 1, p. 36) to convert the midflame windspeed from DIRECT to the 20-foot windspeed required by SPOT. As illustrated in figure 21, the list for SPOT linked to DIRECT gives the range of midflame windspeeds carried over from DIRECT, the exposed-fuel wind adjustment factor for the fuel model specified in DIRECT, and the resulting range of 20-foot windspeeds that are used in SPOT. Notice that the wind limit is reached in this example. The maximum effective windspeed of 18.2 mi/h is used in the flame length calculations, while the actual windspeed is carried over to SPOT.

Chaparral often burns under Santa Ana wind conditions, resulting in high-intensity line fires. Figure 22 shows predicted flame lengths and spotting distances for a range of fine dead fuel moistures and midflame windspeeds. In the first example, the wind is blowing upslope and the spotting source is midslope on the windward side. In the second example, wind is blowing downslope and the spotting source is midslope on the leeward side. Flame length and spotting distance predictions are, however, nearly the same. This is a wind-driven fire and the slope has very little effect. You are responsible for the consistency between the slope and wind direction input to DIRECT and the terrain description and spotting source location in SPOT. But do not be overly concerned with it. There is much variability in real world terrain as compared to the smooth curve used in the model (fig. 23). Table output from SPOT can be used to examine the effect of a range of values on the predictions.

The maximum spotting distance predictions can be used for both wildfire and for prescribed fire. About all that can be done about the occurrence of spot fires on wildfires is to predict where they might be and to watch for them. Spot fires beyond the main front can be a major factor in safety considerations and crew placement. In the planning stage of prescribed fire, spotting distance predictions can be used to determine acceptable conditions for executing the burn. Predictions can be used to place holding crews when the burn is conducted.

Albini (1983) points out that "because several elements of the model process are both speculative and not subject to direct validation, these results are to be considered tentative. Field tests of the spotting distance predictions are sought as a means of testing the utility of the model." Keep in mind that these predictions are for **maximum** spotting distances, and that most firebrands are not expected to travel that distance.

MAP DISTANCE (MAP)

MAP is an independent module in the FIRE1 program that translates calculated distances to measurements that can be plotted on a map. These may be spread distance from SIZE, maximum spotting distance from SPOT, or rate of spread from DIRECT or SITE. The map scale can be specified as either representative fraction or as inches per mile or centimeters per kilometer.

Figure 24 shows the equivalent map distance for three values of maximum spotting distance. Figure 25 shows the map spread distance for various values of rate of spread and elapsed time.

SLOPE (SLOPE, PERCENT, AND DEGREES)

A value for slope is used in the spread and intensity calculations in DIRECT and SITE. DIRECT requires direct input of the slope value. SITE either accepts the value directly or offers the option of calculating it from map measurements as described in Part 1, p. 38. We now offer the independent keyword SLOPE in the FIRE1 program for calculating slope value from topographic map measurements.

Calculation of slope steepness is based on map scale, contour interval, and the number of contour intervals over a specified map distance. Figure 26 shows calculated slope values in percentage and then degrees.

MAP	
1MAP SCALE, IN/MI	3 .0 0
	1:21120
2UNITS OPTION	2.=SPOT DISTANCE
4SPOT DISTANCE, MI	1.0 2.0 3.0

	(V4.0)	
SPOT	I	MAP
DISTANCE	I	SPOT FIRE
	I	DISTANCE
(MI)	I	(IN)
	I	
1.	I	3.0
	I	
2.	I	6.0
	I	
3.	I	9.0

Figure 24—Example MAP run to convert spotting distance to map distance.

MAP	
1MAP SCALE, IN/MI	2.00
	1:31680
2UNITS OPTION	3.=RATE OF SPREAD
5RATE OF SPREAD, CH/H	20.0 30.0 40.0 50.0
6ELAPSED TIME, HR	.5 1.0 1.5 2.0

MAP SPRE	=== AD	DISTANCE,	IN		-=====	(V4.0)
RATE OF	I T	ELA	PSED	TIME, HR		
SPREAD (CH/H)	I T.	•5	1.0	1.5	2.0	
20.	Ī	•3	.5	.8	1.0	
	I	.4	.8		1.5	
30.	I					
40.	I	.5	1.0		2.0	
50.	Ι	.6	1.3	1.9	2.5	

Figure 25—Example MAP run to convert rate of spread and elapsed time to map distance.

	IR IN	IN/MI TERVAL, FT CE, IN	2.64 1:24000 20.0 .4						
4NUMBEF	CON	TOUR INTERVALS	10.0 20.0	30.0 40.0	50.0				
(V	74.0)								
NUMBER	I								
OF	I	TERRAIN	ELEVATION	HORIZONTAL					
CONTOUR	Ι	SLOPE	CHANGE	DISTANCE					
INTERVLS	I	(%)	(FT)	(FT)					
10.	I	25.	200.	800.					
10.	Ī	-2.							
20.	I	50.	400.	800.					
30.	I	75.	600.	800.					
50.	Ī	17.							
40.	I	100.	800.	800.					
	- <u>I</u> -	100	1000.	800.					
50.	I	125.	1000.	000.					
7)	<i>1</i> 4.0)								
NUMBER	I								
OF	I	TERRAIN	ELEVATION	HORIZONTAL DISTANCE					
CONTOUR	I	SLOPE (DEG)	CHANGE (FT)	(FT)					
INTERVLS	I	(DEG)	(£1)	(11)					
10.	Ī	14.	200.	800.					
-	<u> </u>								

400.

600.

800.

1000.

800.

800.

800.

800.

SLOPE

20.

30.

40.

50.

Ι

Figure 26-Example SLOPE run, first under the mode PERCENT, then under the mode DEGREES.

27.

37.

45.

51.

400 FT 270 800 FT 100 • tan (27°) = 100 • $\frac{400}{800}$ = 50% 800 FT 45° 800 FT $100 \cdot \tan (45^{\circ}) = 100 \cdot \frac{800}{800} = 100\%$ Figure 27-A 27-degree slope is equivalent to a 50-percent slope; 45

degrees is equivalent to 100 percent.

In the earlier version of the program, slope was always specified as percentage. This is the standard in the United States, but some prefer to use degrees. The keywords PERCENT and DEGREES are used to set the mode. The default mode is PERCENT. The mode can be changed at any time, and remains in effect until it is changed again. The keyword DEGREES was entered between the two runs in figure 26.

Notice in figure 26 that a 27-degree slope is equivalent to a 50-percent slope; 45 degrees is equivalent to 100 percent. Those two cases are diagramed in figure 27.

PROBABILITY OF IGNITION (IGNITE)

The IGNITE module of the FIRE2 program allows calculation of probability that a firebrand will ignite forest fuels, given 1-hour fuel moisture, ambient air temperature, and shading of fuels due to cloud and canopy cover. An IGNITE run is shown in figure 28.

As shown in figure 3, IGNITE is an independent module in the FIRE2 program. It is, however, also automatically part of the MOISTURE module, which is described in the next section. Because the input values for IGNITE are already available from MOISTURE, probability of ignition is always given as an output value.

The equation used to calculate probability of ignition was developed by Schroeder (1969). It is based on fuel temperature and moisture content. The method of obtaining fuel temperature is handled differently in the independent module IGNITE than in the automatic probability of ignition calculations in MOISTURE. IGNITE calculations result in the same values as the table given by Rothermel (1983, p. 106). Depending on the shade category, a fixed value is added to air temperature to get fuel temperature. When probability of ignition is calculated as part of MOISTURE, fuel temperature is found using more sophisticated methods that are part of the moisture model (Rothermel and others 1986).

IGNITE							
1DRY BULB TEMPERATURE, F	40.0	60.0	80.0	100.0	120.0		
21-HR FUEL MOISTURE, %	2.0	4.0	6.0	8.0	10.0	12.0	14.0
3FUEL SHADING, %	40.0						

PROBABILITY	OF	IGNITION	, %					(V4.0)
DRY BULB	I	1-	HR FUEL	MOISTU	RE, %			
TEMP (F)	Ī	2.	4.	6.	8.	10.	12.	14.
(1)	T -							
40.0	I	90.	70.	50.	40.	30.	20.	10.
60.0	Ī	90.	70.	50.	40.	30.	20.	20.
80.0	Ī	100.	80.	60.	40.	30.	20.	20.
100.0	Ī	100.	80.	60.	50.	40.	30.	20.
120.0	Ī	100.	90.	70.	50.	40.	30.	20.

Figure 28—Example IGNITE run.

Probability of ignition is the chance that an ignition will result if a firebrand lands on flammable material and that its heat is efficiently and rapidly transferred to the fuel (Schroeder 1969). That is, for probability of ignition of 80 percent, 80 of 100 firebrands will cause ignitions, all conditions being equal and fitting the assumptions of the model. But the probability that an ember might ignite receptive fuel is only one aspect of the spotting problem. There remain questions on whether firebrands are produced, how many, what size and shape, where they land, and so on. (As described in a previous section, the SPOT module of the FIRE1 program predicts maximum spotting distance.)

Although probability of ignition of 80 percent may not tell you how many spot fires will occur, it is an indication of the severity of the situation. Probability of ignition of 80 percent certainly indicates a more severe situation than probability of ignition of 20 percent. Most mathematical models in BEHAVE give predictions in absolute terms: rate of spread in chains per hour, flame length in feet, spotting distance in miles, and so on. Probability of ignition is a percentage. But there are so many unknowns (as described above) that interpretation must largely be based on your experience. This may be in terms such as "little chance of spot fires," "probable spot fires," or "spot fires likely if firebrands are being generated."

Ignition Component (IC), a component of the National Fire Danger Rating System (Deeming and others 1977), is sometimes confused with probability of ignition. Probability of ignition includes a calculation of the heat of preignition, the net amount of heat necessary to raise the temperature of a fuel particle from its initial temperature to

its ignition temperature. The model is also based on the results of a study by Blackmarr (1972), who measured the influence of moisture content on the ignitability of slash pine litter by dropping lighted matches onto fuel beds conditioned to different levels of moisture content.

Ignition Component (IC) was designed for rating fire danger. IC is based on probability of ignition. IC also includes a factor derived from the NFDRS fuel model that makes it a better indicator of human-caused fire occurrence. That factor is based on the finding that incidence of human-caused fires increases with windspeeds over 8 mi/h even though windspeed has nothing to do with the ignition process. This is explained by Haines, Main, and Crosby (1973):

If a fire goes out quickly, there will have been a fire start, but not necessarily a **reportable** fire. Debrisburning fires offer a good example. If a firebrand from a trash burner ignites dry grass on a Missouri oakhickory litter area during a calm afternoon, the fire should spread slowly and may be suppressed by the person maintaining the burner. On a windy day, however, the fire may escape and the operator will have to call for the assistance of a fire suppression unit.

The concept of "reportable" fires is important to rating the fire danger for a large area so that the impact on a fire suppression organization can be estimated. On the other hand, for a specific prescribed fire or wildfire, all ignitions are important. We are concerned with the probability that a firebrand will result in an ignition beyond the fire front or control line. Therefore, Ignition Component is used for fire danger rating; probability of ignition is used for fire behavior prediction.

FINE DEAD FUEL MOISTURE (MOISTURE)

The MOISTURE module of the FIRE2 program and the SITE module of the FIRE1 program are both based on the fine dead fuel moisture model (Rothermel and others 1986). Although all fine dead fuels (0- to \(^1/4\)-inch diameter) are not technically 1-hour timelag (Anderson 1985), we continue to use the currently accepted naming convention, 1-hour.

SITE allows a single calculation of rate of spread, flame length, and intensity with 1-hour moisture content as an intermediate value (Part 1, p. 8). MOISTURE is used to calculate only 1-hour moisture content, offering both table and graphic output. Because of the similarities between SITE and MOISTURE, the same input/output sheet is used for both. Items that apply only to SITE or to MOISTURE are so noted. (The line numbers for SITE have changed from those given in Part 1.)

Because the fine dead fuel moisture model is described in detail in Part 1 (p. 28-35), only an overview is given here. A general flow diagram of the model is shown in figure 29. There are five moisture initialization options to obtain an estimate of the moisture on the previous day. Choice of the option depends on available information. Two examples are direct entry of the moisture value and calculation based on up to 7 days of complete weather. An estimate of the shade is obtained from cloud cover, canopy cover, tree shape, time of year and day, latitude, elevation, and aspect. The moisture content is first calculated for the early afternoon period. Moisture can be calculated for other times of the day based on input of additional weather. A summary of the input requirements is given in Part 1 (fig. 13, p. 34). For the purposes of this model, a day goes from 1200 to 1200 (noon to noon) rather than from midnight to midnight.

MOISTURE offers two run options: burn time calculations and hourly calculations. The first option gives calculated values for the specified burn time. A range of values can be entered for one or two input values in order to produce lists or tables of output values. (SITE does not allow ranges for input variables.) The second option results in hourly values presented in the form of a list or

graphs. The hourly values are intermediate values calculated each hour from 1200 to the specified burn time (see Part 1, fig. 14, p. 35). Single values must be assigned to each input for this option.

Burn Time Calculations

Of the 59 possible input values to MOISTURE, 31 are allowed to vary for the table option. You must choose one or two at a time. The choice is narrowed considerably depending on your objective. If you are interested in looking at different fire locations, you will vary site descriptions such as elevation or aspect. If you want to look at the effect of different conditions on the same fire you will vary the weather input.

When doing runs to see the effect of the change of an input value on the results, be careful about making generalizations. In one case there may be little or no effect, but in another a change in that input may be critical. Easterling and others (1986) did a sensitivity analysis of the model and concluded: "combinations of factors have more direct effect on fine fuel moisture than do single factors. Because of the importance of the interaction of minor factors, it is not recommended that any of the model inputs be dropped due to low model sensitivity."

Figure 30 is a MOISTURE run for a range of crown closure values. This example is for fuel model 2 (timber—grass and understory) and a burn time of 1500. Intermediate values from the model are given in addition to 1-hour fuel moisture. As described in a previous section, probability of ignition is always given as an output with MOISTURE because all of the required input are available. Notice the relationship between crown closure and shade. Shade is used in the calculation of fuel level temperature and relative humidity.

Figure 31 is a MOISTURE run for a range of temperature and relative humidity values at burn time. This is a prediction for fuel model 5 (2-foot brush) with no overstory and a burn time of 1500. For this example tables are printed for 1-hour moisture and for probability of ignition. Moisture values are given to a tenth of a percent so that you can see the trends in the predictions. The nearest percentage is good enough for application.

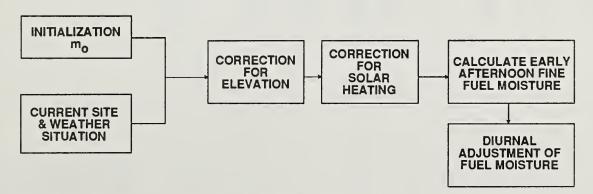


Figure 29—General flow diagram of the fine fuel moisture model that is in SITE and MOISTURE.

1	vî.	n	Т	9	т	1	IR	F

MOISIUME	
1RUN OPTION	1=BURN TIME CALCULATIONS
2MONTH OF BURN	8.
3DAY OF BURN	21.
4LATITUDE	47. N
5BURN TIME (2400 HOURS)	1500.
,,	508.=TIME OF SUNRISE
	1851.=TIME OF SUNSET
6FUEL MODEL	2 = TIMBER (GRASS AND UNDERSTORY)
O TOBE MODEL	2 - IIMBEN (GNASS AND UNDERSTORI)
11TERRAIN SLOPE, %	E0 0
12ELEVATION OF FIRE	50.0
	2000 0
LOCATION, FT	3000.0
13ELEVATION OF WEATHER	
OBSERVATIONS, FT	SAME AS FIRE LOCATION
14ASPECT	S
15CROWN CLOSURE, %	.0 10.0 20.0 30.0 40.0 50.0 60.0
16FOLIAGE	PRESENT
17SHADE TOLERANCE	TOLERANT
18DOMINANT TREE TYPE	1=CONIFEROUS
19AVERAGE TREE HEIGHT, FT	60.0
20RATIO OF CROWN LENGTH	
TO TREE HEIGHT	.5
21RATIO OF CROWN LENGTH	•,
TO CROWN DIAMETER	3.0
TO OHOMN DIMMETER	3.0
22BURN DAY 1400 TEMP, F	80.0
23BURN DAY 1400 RH, %	
24BURN DAY 1400 20-FOOT	30.0
WIND SPEED, MI/H	5.0
25BURN DAY 1400 CLOUD	
COVER, %	.0
26BURN DAY 1400 HAZINESS	2=AVERAGE CLEAR FOREST ATMOSPHERE

BURN TIME WEATHER = 1400 WEATHER

40--EXPOSURE OF FUELS TO

43--MOISTURE INITIALIZATION CODE-----

4=INCOMPLETE WEATHER DATA NO RAIN THE WEEK BEFORE THE BURN WEATHER PATTERN HOLDING

CROWN CLOSURE (%)	(V4.0) I 1-HF I FUEL I MOIS I (%)	BULB TEMP	AIR RH (%)	FUEL LEVEL TEMP (F)	FUEL LEVEL RH (%)	MID- FLAME WIND (MI/H)	FUEL LEVEL WIND (MI/H)	SHADE	PROB OF IGN (%)
0.	I 4.2	80.	30.	109.	11.	1.5	1.0	0.	70.
10.	I 4.4	80.	30.	103.	14.	1.5	•9	17.	70.
20.	I 5.0	80.	30.	96.	18.	1.5	.9	33.	60.
30.	I 5.8	80.	30.	90.	22.	1.5	.9	48.	60.
40.	I 6.8	80.	30.	84.	26.	1.5	.9	61.	50.
50.	I 7.7	80.	30.	80.	30.	1.5	.9	72.	40.
60.	I 7.7	80.	30.	80.	30.	1.5	.9	81.	40.

Figure 30—Example MOISTURE run for a range of crown closure values. Note the relationship between crown closure and percent shade.

MOISTURE 1RUN OPTION	25. 40. N
11TERRAIN SLOPE, %	10.0
12ELEVATION OF FIRE LOCATION, FT	2500.0
13ELEVATION OF WEATHER OBSERVATIONS, FT	
14ASPECT	SE
15CROWN CLOSURE, %	.0
22BURN DAY 1400 TEMP, F 23BURN DAY 1400 RH, %	50.0 60.0 70.0 80.0 90.0 100.0 20.0 30.0 40.0 50.0 60.0 70.0
24BURN DAY 1400 20-FOOT WIND SPEED, MI/H	10.0
25BURN DAY 1400 CLOUD COVER, %	.0
26BURN DAY 1400 HAZINESS	1=VERY CLEAR SKY
BURN TIME WEATHER = 1	400 WEATHER
40EXPOSURE OF FUELS TO THE WIND	1=EXPOSED .4=WIND ADJUSTMENT FACTOR

4=INCOMPLETE WEATHER DATA

WEATHER PATTERN HOLDING

NO RAIN THE WEEK BEFORE THE BURN

Figure 31—Example MOISTURE run for ranges of burn time temperature and relative humidity.

43--MOISTURE INITIALIZATION

CODE-----

1-HR FUEL MO		======= RE, %					=====	(V4.0)
BURN TIME	I I	BURN	TIME	RELATIV	E HUMID	ITY, %		
TEMP (F)	I I	20.	30.	40.	50.	60.	70.	
50.	I I I	4.2	5.7	7.0	8.1	9.0	9.6	
60.	_	4.2	4.6	5.6	6.6	7.5	8.4	
70.	I I	4.2	4.5	5.4	6.3	7.1	7.9	
80.		4.2	4.4	5.3	6.0	6.8	7.5	
90.	Ī	4.2	4.4	5.1	5.9	6.5	7.2	
100.	I	4.1	4.4	5.1	5.7	6.3	6.9	
PROBABILITY		•	%					(V4.0)
BURN TIME	I I			RELATIV				
TEMP (F)	Ī	20.	30.	40.	50.	60.	70.	
50.	I I I	60.	50.	40.	40.	30.	30.	
60.	I I	70.	60.	60.	50.	40.	40.	
70.	I	70.	70.	60.	50.	50.	40.	
80.	I	70.	70.	60.	60.	50.	50.	
90.	I	80.	70.	70.	60.	50.	50.	
100.	I	80.	80.	70.	60.	60.	50.	

Figure 31 (Con.)

Hourly Calculations

In order to calculate fuel moisture at burn time, calculations are done for each hour starting at 1200. The hourly calculation option of MOISTURE allows you to examine those values, in the form of either a table or a graph. Because this is essentially one set of calculations, a single value is required for each input. Because a burn day goes from 1200 to 1200, in order to see a 24-hour prediction, you must enter a burn time from the interval 1100 to 1159.

Figure 32 gives a MOISTURE run under the hourly calculation option for a burn time of 1100. One of the output choices is a table listing of the hourly values from 1200 to burn time. Any of the values on that table can be plotted. We show here only the 1-hour moisture plot. The graph is not smooth because of the resolution of the character-type graph. We have sketched in a smooth curve. Sunrise and sunset are denoted on the graph by R and S.

Appendix A includes complete runs of the MOISTURE module showing questions and user response.

RELATIVE HUMIDITY (RH)

The RH module determines relative humidity and dew point from wet bulb and dry bulb temperatures and elevation. This is an alternative to using tables such as those in the S-390 Fire Behavior Field Guide, p. 19-33 (National Wildfire Coordinating Group 1981). But because the RH module uses equations, the results may be slightly different.

Figure 33 shows tables of relative humidity and dew point for ranges of wet bulb and dry bulb temperatures. Wet bulb temperature must be greater than the dry bulb temperature as indicated by the -888. values in the upper right corner of the tables. At the lower left corner, -999. values indicate that the calculated dew point is too low for valid calculations.

MOISTURE	
1RUN OPTION	2=HOURLY CALCULATIONS (GRAPHIC OUTPUT)
2MONTH OF BURN	2.
3DAY OF BURN	10.
4LATITUDE	33. N
5BURN TIME (2400 HOURS)	1100.
	639.=TIME OF SUNRISE
	1720.=TIME OF SUNSET
6FUEL MODEL	7 = SOUTHERN ROUGH
1TERRAIN SLOPE, %	.0
2ELEVATION OF FIRE	
LOCATION, FT	300.0
3ELEVATION OF WEATHER	
OBSERVATIONS, FT	SAME AS FIRE LOCATION
5CROWN CLOSURE, %	50.0
6FOLIAGE	-
	ABSENT
8DOMINANT TREE TYPE	2=DECIDUOUS
9AVERAGE TREE HEIGHT, FT	50.0
20RATIO OF CROWN LENGTH	
TO TREE HEIGHT	•5
21RATIO OF CROWN LENGTH	
TO CROWN DIAMETER	1.0
2BURN DAY 1400 TEMP, F	80.0
3BURN DAY 1400 RH, %	60.0
24BURN DAY 1400 20-FOOT	00.0
	5 0
WIND SPEED, MI/H	5.0
25BURN DAY 1400 CLOUD	40.0
COVER, %	10.0
26BURN DAY 1400 HAZINESS	3=MODERATE FOREST BLUE HAZE
27SUNSET TEMPERATURE, F	70.0
28SUNSET RH, %	60.0
29SUNSET 20-FOOT	3313
WIND SPEED, MI/H	.0
30SUNSET CLOUD COVER, %	30.0
JO-SUNSET CLOUD COVER, /	30.0
31SUNRISE TEMPERATURE, F	60.0
2SUNRISE RH, %	60.0
9SUNRISE 20-FOOT	
WIND SPEED, MI/H	.0
4SUNRISE CLOUD COVER, %	.0
TE BOINTED OLOOD COVIET, A	••
35BURN TIME TEMPERATURE, F	60.0
36BURN TIME RH, %	50.0
37BURN TIME 20-FOOT	90.0
	0
WIND SPEED, MI/H	.0
38BURN TIME CLOUD COVER, %	.0
39BURN TIME HAZINESS	3=MODERATE FOREST BLUE HAZE
10EXPOSURE OF FUELS TO	0 DADETALLIA OVER 1995-
THE WIND	2=PARTIALLY SHELTERED
	.3=WIND ADJUSTMENT FACTOR
43MOISTURE INITIALIZATION	
CODE	1=1-HR FUEL MOISTURE KNOWN FOR BURN DAY
44BURN DAY -1 1-HR FUEL	1-1 IN TODE NOTOTORE KNOWN FOR DUNN DAT
MOISTURE, %	9.0
MOTOTORIE, /	J. U

Figure 32—Example MOISTURE run under the hourly output option. A table of hourly values and a plot of 1-hour fuel moisture are given.

(VERSION 4.0)									
1-HR	DRY	AIR	FUEL	FUEL	MID-	FUEL	SHADE	PROB	
FUEL	BULB	RH	LEVEL	LEVEL	FLAME	LEVEL		OF	
	TEMP		TEMP	RH	WIND	WIND		IGN	
		(%)	(F)		(MI/H)	(MI/H)	(%)	(%)	
	80.	60.	92.	40.	1.5	.8	14.	40.	
	80.	60.	92.	40.	1.5		14.	40.	
			92.		1.5	.8	14.	40.	
9.0	79.	60.		47.	1.1	.6	22.	30.	
		60.		55.	.6	.3	31.	30.	
	72.				.2	.1	55.	30.	
	69.				.0	.0	100.	30.	
					.0	.0		20.	
					.0	.0		20.	
					.0	.0		20.	
						.0		20.	
						.0		20.	
					.0	.0		20.	
					.0	.0		20.	
					.0	.0	100.	20.	
					.0	.0	100.	20.	
					.0	.0	100.	20.	
					.0	.0		20.	
					.0	.0	100.	20.	
		60.		60.	.0	.0	39 •	20.	
-		59•	64.	51.	.0	.0	11.	20.	
		57•	73.	37•	.0	.0	7.	20.	
12.2	60.	54.	81.	27.	.0	.0	5.	20.	
11.3	60.	50.	86.	21.	.0	.0	4.	20.	
	1-HR FUEL MOIS (%) 8.9 8.9 9.0 9.4 9.9 10.2 10.6 10.9 11.1 11.4 11.6 11.8 12.1 12.2 12.4 12.6 12.7 12.9 13.0 12.8 12.2	1-HR DRY FUEL BULB MOIS TEMP (%) (F) 8.9 80. 8.9 80. 9.0 79. 9.4 76. 9.9 72. 10.2 69. 10.6 68. 10.9 67. 11.1 66. 11.4 65. 11.6 64. 11.8 63. 12.1 62. 12.2 61. 12.4 61. 12.6 60. 12.7 60. 13.0 60. 13.0 60. 13.0 60. 12.8 60. 12.2 60.	1-HR DRY AIR FUEL BULB RH MOIS TEMP (%) (F) (%) 8.9 80. 60. 8.9 80. 60. 9.0 79. 60. 9.4 76. 60. 10.2 69. 60. 10.6 68. 60. 10.9 67. 60. 11.1 66. 60. 11.4 65. 60. 11.4 65. 60. 11.8 63. 60. 12.1 62. 60. 12.2 61. 60. 12.4 61. 60. 12.4 61. 60. 12.5 60. 60. 12.7 60. 60. 12.9 60. 60. 13.0 60. 60. 13.0 60. 59. 12.8 60. 57. 12.2 60. 54.	1-HR DRY AIR FUEL FUEL BULB RH LEVEL MOIS TEMP (%) (F) (%) (F) 8.9 80. 60. 92. 8.9 80. 60. 92. 9.0 79. 60. 86. 9.4 76. 60. 78. 9.9 72. 60. 72. 10.2 69. 60. 69. 10.6 68. 60. 68. 10.9 67. 60. 67. 11.1 66. 60. 66. 11.4 65. 60. 65. 11.6 64. 60. 65. 11.6 64. 60. 64. 11.8 63. 60. 63. 12.1 62. 60. 62. 12.2 61. 60. 61. 12.4 61. 60. 61. 12.4 61. 60. 61. 12.5 60. 60. 60. 12.7 60. 60. 60. 12.9 60. 60. 60. 13.0 60. 60. 60. 13.0 60. 59. 64. 12.8 60. 57. 73. 12.2 60. 54. 81.	1-HR DRY AIR FUEL FUEL FUEL BULB RH LEVEL LEVEL MOIS TEMP TEMP RH (%) (F) (%) (F) (%) 8.9 80. 60. 92. 40. 8.9 80. 60. 92. 40. 8.9 80. 60. 92. 40. 9.0 79. 60. 86. 47. 9.4 76. 60. 72. 60. 10.2 69. 60. 69. 60. 10.2 69. 60. 69. 60. 10.6 68. 60. 68. 60. 10.9 67. 60. 67. 60. 11.1 66. 60. 66. 60. 11.4 65. 60. 65. 60. 11.4 65. 60. 65. 60. 11.8 63. 60. 63. 60. 12.1 62. 60. 62. 60. 12.2 61. 60. 61. 60. 12.4 61. 60. 61. 60. 12.5 60. 60. 60. 60. 12.7 60. 60. 60. 60. 12.9 60. 60. 60. 60. 12.9 60. 60. 60. 60. 13.0 60. 60. 60. 60. 13.0 60. 59. 64. 51. 12.8 60. 57. 73. 37. 12.2 60. 54. 81. 27.	1-HR DRY AIR FUEL FUEL MID- FUEL BULB RH LEVEL LEVEL FLAME MOIS TEMP TEMP RH WIND (%) (F) (%) (F) (%) (MI/H) 8.9 80. 60. 92. 40. 1.5 8.9 80. 60. 92. 40. 1.5 8.9 80. 60. 92. 40. 1.5 9.0 79. 60. 86. 47. 1.1 9.4 76. 60. 72. 602 10.2 69. 60. 69. 600 10.6 68. 60. 69. 600 10.9 67. 60. 67. 600 11.1 66. 60. 66. 600 11.4 65. 60. 65. 600 11.8 63. 60. 63. 600 11.8 63. 60. 63. 600 12.1 62. 60. 62. 600 12.2 61. 60. 61. 600 12.4 61. 60. 61. 600 12.5 60. 60. 60. 600 12.7 60. 60. 60. 60. 600 12.9 60. 60. 60. 600 13.0 60. 60. 60. 600 13.0 60. 59. 64. 510 12.8 60. 57. 73. 370 12.8 60. 57. 73. 370 12.8 60. 54. 81. 270	1-HR DRY AIR FUEL FUEL MID- FUEL FUEL BULB RH LEVEL LEVEL FLAME LEVEL MOIS TEMP RH WIND WIND WIND (%) (F) (%) (MI/H) (MI/H) (MI/H) 8.9 80. 60. 92. 40. 1.5 .8 8.9 80. 60. 92. 40. 1.5 .8 8.9 80. 60. 92. 40. 1.5 .8 8.9 80. 60. 92. 40. 1.5 .8 8.9 80. 60. 92. 40. 1.5 .8 9.0 79. 60. 86. 47. 1.1 .6 9.4 76. 60. 72. 60. .2 .1 10.2 69. 60. 69. 60. .0 .0 11.4 65. 60.	1-HR DRY AIR FUEL LEVEL LEVEL LEVEL FLAME LEVEL FLAME LEVEL FLAME LEVEL FLAME LEVEL WIND WIND SHADE FUEL LEVEL FLAME LEVEL FLAME LEVEL WIND WIND SHADE FLAME LEVEL WIND WIND COMMITTEN COMMITTEN	

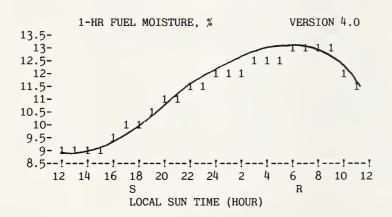


Figure 32 (Con.)

RH
1--DRY BULB TEMPERATURE, F
2--WET BULB TEMPERATURE, F
3--ELEVATION, FT
65.0 70.0 75.0 80.0 85.0 90.0 95.0 60.0 65.0 70.0 75.0 80.0 80.0

RELATIVE HUMIDITY, % (V4.0)									
DRY I	WE	r BULB	TEMPERA	TURE,	DEG F				
TEMP (F)	I I-	50.	55 •	60.	65.	70.	7 5.	80.	
65.	I	33.	53.	76.	100.	-888.	-888.	-888.	
70.	I I I	21.	38.	5 7 •	77.	100.	-888.	-888.	
7 5•	I	12.	26.	42.	59.	79.	100.	-888.	
80.	Ī	5.	17.	30.	45.	62.	80.	100.	
85.	I I	-999•	10.	22.	34.	48.	63.	81.	
90.	Ī	-999.	5.	15.	25.	37.	50.	65.	
95.	Ī	-999.	1.	10.	19.	29.	40.	53.	

-888 = WET BULB TEMPERATURE GREATER THAN DRY BULB.

-999 = DEW POINT IS LESS THAN -40 DEGREES.

DEW POINT, F	S#2				:			(V4.0)
DRY I	I	WET	BULB	TEMPERA	TURE,	DEG F		
TEMP (F)	I T-	50.	55.	60.	65.	70.	75 •	80.
	Ī	- 4	1.0		-	000	000	000
65.	I	36.	48.	57.	65.	-888.	-888.	-888.
70.	Ī	29.	43.	54.	63.	70.	-888.	-888.
75•	Ī	19.	38.	50.	60.	68.	75.	-888.
80.	I	4.	32.	46.	57.	66.	73.	80.
85.	I I I	-999.	23.	42.	54.	63.	71.	78.
90.	I	-999.	11.	36.	50.	60.	69.	77.
95.	Ī	-999.	-14.	29.	46.	58.	67.	75.

-888 = WET BULB TEMPERATURE GREATER THAN DRY BULB.

-999 = DEW POINT IS LESS THAN -40 DEGREES.

Figure 33—Example RH run.

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APPENDIX A—ANNOTATED RUNS OF THE FIRE1 AND FIRE2 PROGRAMS OF BEHAVE.

Fire behavior prediction models that have been added to BEHAVE are illustrated in the body of the paper with sample input and output from the programs. This appendix provides complete user sessions for the FIRE1 and FIRE2 programs, with all of the interaction between the user and the computer. Basic operation is emphasized in the sample run in appendix A of Part 1 (Andrews 1986); that information is still valid. This run is used to illustrate the changes and additions to the programs.

Lines that begin with a > (the prompt symbol) were typed by the user. All others were printed by the computer. The prompt symbol may be different on another computer. (The Forest Service Data General system does not give a prompt.)

Gaining access to the BEHAVE programs and printing log files are functions of the computer being used and therefore are not described in this manual.

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WELCOME TO THE BEHAVE SYSTEM BURN SUBSYSTEM

FIRE1 PROGRAM: VERSION 4.0 -- MAY 1989

DEVELOPED BY: THE FIRE BEHAVIOR RESEARCH WORK UNIT

INTERMOUNTAIN FIRE SCIENCES LABORATORY

MISSOULA, MONTANA

YOU ARE RESPONSIBLE FOR SUPPLYING VALID INPUT AND FOR CORRECTLY INTERPRETING THE FIRE BEHAVIOR PREDICTIONS

This is important.

ASSUMPTIONS, LIMITATIONS, AND APPLICATION OF MATHEMATICAL
MODELS USED IN THIS PROGRAM ARE IN:
Andrews, Patricia L. "BEHAVE: Fire behavior prediction and
fuel modeling system--BURN subsystem, Part 1", INT-GTR-194, 1986
Andrews, Patricia L., and Chase, Carolyn H. "BEHAVE: Fire
behavior prediction and fuel modeling system--BURN
subsystem, Part 2", INT-GTR-260, 1989

(PRESS CARRIAGE RETURN TO CONTINUE)

PAUSE OPTION AND ENGLISH UNITS SET.

SLOPE MEASUREMENT IN PERCENT.

WHEN YOU ARE READY TO CONTINUE AFTER THE PROMPT
SYMBOL IS PRINTED WITHOUT A QUESTION,
PRESS THE CARRIAGE RETURN KEY.

TYPE 'CUSTOM' IF YOU ARE GOING TO USE CUSTOM FUEL MODELS.

FIRE1 KEYWORD?

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT,
MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM,
TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
ENGLISH, METRIC, PERCENT, DEGREES,
COMMENT, KEY, HELP, STATUS, QUIT

>status

****ALL UPPER CASE PLEASE****

FIRE1 KEYWORD?

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH SPOT,
MORTALITY MAP SLOPE DISPATCH, CUSTOM,
TERSE, WORDY, PAUSE, NOPAUSE, LOG NOLOG
ENGLISH METRIC PERCENT DEGREES
COMMENT KEY, HELP STATUS QUIT

>STAT

The sprogram recognizes only upper case input. Use your shift lock key.

These are new Reywords.

The program Checks only the first four letters of keywords.

**** FIRE1 STATUS REQUEST **** PROMPT MODE : WORDY DISPLAY MODE : PAUSE LOG FILE NAME : UNDECLARED LOG FUNCTION : OFF FUEL FILE NAME: UNDECLARED DISPLAY UNITS : ENGLISH SLOPE UNITS : PERCENT FIRE1 KEYWORD? ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT, MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,	Default values for mode keywords.
ENGLISH, METRIC, PERCENT, DEGREES,	On non-printing
COMMENT, KEY, HELP, STATUS, QUIT	terminals, COMMENT is
COMMENT	useful only if the LOG
NO LOG FILE CURRENTLY ACTIVE. REMEMBER THA COMMENT APPEARS ONLY ON YOUR TERMINAL NO	T THIS option is activated. How.
ENTER TEXT FOR DOCUMENTATION.	gwee you the choice of
USE A CARRIAGE RETURN AT THE END OF EACH	LINE.
TO TERMINATE, ENTER (ON A NEW LINE) **	continuing of you are
FOLLOWED BY A CARRIAGE RETURN.	using a printing terminal.
************	*******
COMMENT:	
**	<u></u>
******	0 . , , , , , , , , , , , , , , , , , ,
FIRE1 KEYWORD?	Let's terminate the Comment
ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT, MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH, METRIC, PERCENT, DEGREES, COMMENT, KEY, HELP, STATUS, QUIT	and specify a log file.
LOG	
WHAT FILE NAME DO YOU WANT TO USE? (12 CHAR FIRST CHARACTER MUST BE ALPHABETIC. FOLL CONVENTION FOR YOUR COMPUTER.	OW THE NAMING
LOGFIL	This is a new file. Specifying an existing file will be
LOG IS ON.	an existing the write to
THE NAME OF YOUR LOGFILE IS: (LOGFIL)	

FIRE1 KEYWORD?

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT, MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH, METRIC, PERCENT, DEGREES, COMMENT, KEY, HELP, STATUS, QUIT

has been attached to the run, it remains the same until the run is terminated.

STATUS

**** FIRE1 STATUS REQUEST ****

PROMPT MODE : WORDY DISPLAY MODE : PAUSE

LOG FILE NAME : LOGFIL

LOG FUNCTION : ON -FUEL FILE NAME: UNDECLARED

DISPLAY UNITS : ENGLISH SLOPE UNITS : PERCENT

FIRE1 KEYWORD?

ENTER DIRECT.SITE.SIZE.CONTAIN.SCORCH.SPOT. MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH, METRIC, PERCENT, DEGREES, COMMENT, KEY, HELP, STATUS, QUIT

> COMMENT

ENTER TEXT FOR DOCUMENTATION.

USE A CARRIAGE RETURN AT THE END OF EACH LINE. TO TERMINATE, ENTER (ON A NEW LINE) ** FOLLOWED BY A CARRIAGE RETURN.

à log file has been declared.

The log function can be turned on and off at any time during the run.

Characters typed after the 80 m and syole a return will be lost (even if the Cursor automatically moves to the next line).

COMMENT:

>AN FBA MIGHT USE THE COMMENT KEYWORD TO LABEL A DIRECT RUN WITH

1. FIRE NAME

2. PROJECTION TIME AND DATE

FIRE1 KEYWORD?

ENTER DIRECT.SITE.SIZE.CONTAIN.SCORCH.SPOT. MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH, METRIC, PERCENT, DEGREES, COMMENT, KEY, HELP, STATUS, QUIT

One suggestion for the use of comment. Use it however you wish.

>SLOPE

SLOPE KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH . METRIC . PERCENT . DEGREES . COMMENT, KEY, HELP, STATUS

> INPUT

(1) MAP SCALE OPTION ? 1-2 OR QUIT 1=REPRESENTATIVE FRACTION 2=INCHES PER MILE

> 2

(1) MAP SCALE, IN/MI ? .1-20

Input to the hundredths place is OK only for map scale and precipitation amount.

*(2) CONTOUR INTERVAL, FT ? 10-500 >40

*(3) MAP DISTANCE, IN ? .1-10

>1

*(4) NUMBER OF CONTOUR INTERVALS ? 1-100 >5,9,2 * byone an input prompt indicates that a range of input is ok.

THE FOLLOWING VALUES WILL BE USED

5.0 7.0 9.0

OK ? Y-N

> Y

SLOPE KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

>LIST

SLOPE

1--MAP SCALE, IN/MI----- 2.64

1: 24000.

2--CONTOUR INTERVAL, FT --- 40.0

3--MAP DISTANCE, IN ----- 1.0

4--NUMBER CONTOUR INTERVALS 5.0 7.0 9.0

SLOPE KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> RUN

The version number of the program is printed with all RUN output.

<i>C</i> '	,	1		
NUMBER	I			
OF	1	TERRAIN	ELEVATION	HORIZONTAL
CONTOUR	I	SLOPE	CHANGE	DISTANCE
INTERVLS	1	(%)	(FT)	(FT)
	I			
5.0	I	10.	200.	2000.
	I			
7.0	I	14.	280.	2000.
	I			
9.0	I	18.	360.	2000.
			.3	

SLOPE KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LCG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> DEGREES

Let's look at slope in degrees.

CURRENT UNITS SYSTEM: ENGLISH. SLOPE IS IN DEGREES

SLOPE KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> RUN

(V4.0)				Commonate there and we
NUMBER	I				Compare these values with those marked in
OF	I	TERRAIN	ELEVATION	HORIZONTAL	with those marked in
CONTOUR	I	SLOPE	CHANGE	DISTANCE	the previous run.
INTERVLS	I	(DEG)	(FT)	(FT)	the flavour raise.
	I				
5.0	I	6.	200.	2000.	
	I				
7.0	I	8.	280.	2000.	
	I				
9.0	I	10.	360.	2000.	
		L	,		

SLOPE KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> PERCENT

Back to our usual units.

CURRENT UNITS SYSTEM: ENGLISH. SLOPE IS IN PERCENT

SLOPE KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>QUIT

FINISH SLOPE -- BACK TO FIRE1

```
FIRE1 KEYWORD?
```

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT,

MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS, QUIT

> DIRECT

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

SIZE, SCORCH

> INPUT

- (1) FUEL MODEL ? 0-99 OR QUIT (ENTER 0 FOR TWO FUEL MODEL CONCEPT INPUT.)
- *(2) 1-HR FUEL MOISTURE, % ? 1-60
- *(3) 10-HR FUEL MOISTURE, % ? 1-60
- >6
- *(6) LIVE WOODY MOISTURE, % ? 30-300
- *(7) MIDFLAME WINDSPEED, MI/H ? 0-99 >1,5,1

THE FOLLOWING VALUES WILL BE USED

1.0 2.0 3.0 4.0 5.0

OK ? Y-N

.

> **Y**

*(8) TERRAIN SLOPE, % ? 0-100 >40,100,10

THE FOLLOWING VALUES WILL BE USED

40.0 50.0 60.0 70.0 80.0 90.0 100.0 OK ? Y-N
>Y

- *(9) DIRECTION OF WIND VECTOR,

 DEGREES CLOCKWISE FROM UPHILL ? 0-360
- (10) DO YOU WANT FIRE BEHAVIOR PREDICTIONS FOR THE DIRECTION OF MAXIMUM SPREAD ? Y-N

Link to SCORCH and SPOT is not allowed with the two-fuel-model concept.

You can INPUT in English units ...

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES.

COMMENT, KEY, HELP, STATUS

> METRIC

CURRENT UNITS SYSTEM: METRIC. SLOPE IS IN PERCENT

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>LIST

Note that METRIC and ENGLISH do not affect Slope units.

then Switch to Metric

to run.

DIRECT

1--FUEL MODEL -----5 -- BRUSH, 2 FT (60 CM)

2--1-HR FUEL MOISTURE, % --5.0

3--10-HR FUEL MOISTURE, % -6.0

6--LIVE WOODY MOISTURE, % -90.0

7--MIDFLAME WINDSPEED, KM/H 1.6 3.2 4.8

8--TERRAIN SLOPE, % -----

Non-integer values are due 1.6 3.2 4.8 6.4 8.0 40.0 50.0 60.0 70.0 80.0 90.0 100.0 & Conversion to metric units

9--DIRECTION OF WIND VECTOR 40.0

DEGREES CLOCKWISE

FROM UPHILL

10--DIRECTION OF SPREAD ----

CALCULATIONS

DEGREES CLOCKWISE FROM UPHILL

DIRECTION OF MAXIMUM SPREAD

TO BE CALCULATED

Note you later reference.

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> RUN

TABLE VARIABLE ? 0-7

0=NO MORE TABLES 4=FLAME LENGTH

1=RATE OF SPREAD 5=REACTION INTENSITY

2=HEAT PER UNIT AREA 6=EFFECTIVE WINDSPEED

3=FIRELINE INTENSITY 7=DIRECTION OF MAX SPREAD

FLAME LE	NGTH	, M						(V4.0)
	====								=
MIDFLAME	I	TE	RRAIN S	LOPE, %					
WIND	I								
	I	40.0	50.0	60.0	70.0	80.0	90.0	100.0	
(KM/H)	I								-
	I								
1.6	I	1.3	1.5	1.7	1.9	2.1	2.3	2.5	The flame lengths are in meters.
	I								The factories and the same of
3.2	I	1.5	1.7	1.8	2.0	2.2	2.4	2.6	are in meters.
	I								
4.8	ı	1.7	1.9	2.0	2.2	2.4	2.5	2.7	
	ı								
6.4	ī	2.0	2.1	2.2	2.4	2.5	2.7	2.9	
•••	ī			· -					
8.0	ī	2.2	2.3	2.4	2.5	2.7	2.8	3.0	

TABLE VARIABLE ? 0-7

O=NO MORE TABLES 4=FLAME LENGTH

1=RATE OF SPREAD 5=REACTION INTENSITY

2=HEAT PER UNIT AREA 6=EFFECTIVE WINDSPEED

3=FIRELINE INTENSITY 7=DIRECTION OF MAX SPREAD
>0

IF YOU WANT TO CONTINUE WITH THE AREA AND PERIMETER CALCULATIONS,
TYPE 'SIZE'

IF YOU WANT TO CONTINUE WITH SCORCH HEIGHT CALCULATIONS.

TYPE 'SCORCH'

IF YOU WANT TO CONTINUE WITH SPOTTING DISTANCE FROM A WIND-DRIVEN SURFACE FIRE, TYPE 'SPOT'

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

SIZE, SCORCH, SPOT

> ENGLISH

CURRENT UNITS SYSTEM: ENGLISH. SLOPE IS IN PERCENT.

Back to English units.

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

SIZE, SCORCH, SPOT

> RUN

TABLE VARIABLE ? 0-7

0=NO MORE TABLES 4=FLAME LENGTH

1=RATE OF SPREAD 5=REACTION INTENSITY

2=HEAT PER UNIT AREA 6=EFFECTIVE WINDSPEED

3=FIRELINE INTENSITY 7=DIRECTION OF MAX SPREAD

DIRECTION OF MAXIMUM SPREAD, DEG (V4.0)

MIDFLAME	I	I TERRAIN SLOPE, %								
WIND	1									
	I	40.0	50.0	60.0	70.0	80.0	90.0	100.0		
(MI/H)	I									
	I	(7		
1.0	I	12.	8.	6.	5.	4.	З.	2.		
	I	ı								
2.0	I	21.	17.	13.	10.	8.	7.	6.		
	I				C			1		
3.0	I	27.	22.	19.	16.	13.	11.	9.		
	I									
4.0	I	30.	26.	23.	20.	17.	15.	13.		
	I									
5.0	I	32.	29.	26.	23.	20.	18.	16.		

This will be referred to later.

TABLE VARIABLE ? 0-7

O=NO MORE TABLES 4=FLAME LENGTH

1=RATE OF SPREAD 5=REACTION INTENSITY

2=HEAT PER UNIT AREA 6=EFFECTIVE WINDSPEED

3=FIRELINE INTENSITY 7=DIRECTION OF MAX SPREAD
>0

IF YOU WANT TO CONTINUE WITH THE AREA AND PERIMETER CALCULATIONS, TYPE 'SIZE'

IF YOU WANT TO CONTINUE WITH SCORCH HEIGHT CALCULATIONS,

TYPE 'SCORCH'

IF YOU WANT TO CONTINUE WITH SPOTTING DISTANCE FROM A WIND-DRIVEN SURFACE FIRE, TYPE 'SPOT'

Rink to spot is allowed only for a head fire.

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
ENGLISH, METRIC, PERCENT, DEGREES,
COMMENT, KEY, HELP, STATUS
SIZE, SCORCH, SPOT

SPOT

SPOT-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> INPUT

Keyword requests and lists are labeled to help you keep track of where you are.

*(4) RIDGE/VALLEY ELEVATIONAL DIFFERENCE, FT ? 0-4000

>1000

*(5) RIDGE/VALLEY HORIZONTAL DISTANCE, MI ? 0-4

>1.

(6) SPOTTING SOURCE LOCATION ? 0-3

O=MIDSLOPE, WINDWARD SIDE

1=VALLEY BOTTOM

2=MIDSLOPE, LEEWARD SIDE

3=RIDGETOP

>1

SPOT-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>LIST

Soot linked to DIRECT

3-WIND-DRIVEN SURFACE FIRE Lations applied only when

2.5 5.0 7.5 10.0 12.5 there is no significant

1.0 2.0 3.0 4.0 5.0 timber Cover

& EXPOSED FUEL WAF =

1--FIREBRAND SOURCE-----

2--MEAN COVER HEIGHT, FT --

3--20-FOOT WINDSPEED, MI/H

SPOT-LINKED-TO-DIRECT

4--RIDGE/VALLEY ELEVATION

FROM MIDFLAME WIND =

DIFFERENCE, FT -- 1000.0

5--RIDGE/VALLEY HORIZONTAL

DISTANCE, MI ---- 1.0

6--SPOTTING SOURCE LOCATION 1.-- VALLEY BOTTOM

12--FLAME LENGTH, FT ----- OUTPUT FROM DIRECT. RANGE=

Acured from DIRECT

SPOT-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> RUN

20-jt wind is calculated from midflame wind input in DIRECT and the wind adjustment jactor for the fuel model from DIRECT (does not use effective windspeed)

SPOT input lines 1,2,3,12 cannot be changed in linked runs.

MAXIMUM SPOTTING DISTANCE, MI MIDFLAME I TERRAIN SLOPE. % WIND I I 40.0 50.0 60.0 70.0 80.0 90.0 100.0 (MI/H) 1.0 т -1.0 -1.0 -1.0 -1.0 2.0 . 1 -1.0 -1.0 -1.0 3.0 . 1 . 2 . 2 . 2 . 2 -1.0 4.0 I . 2 . 2 . 2 . 2 . 3 5.0 .3 .3 .3 . 3 . 3

-1.=THIS IS NOT A WIND-DRIVEN HEAD FIRE.

THE DIRECTION OF MAXIMUM SPREAD IS MORE THEN 30

DEGREES FROM THE DIRECTION OF THE WIND VECTOR.

Note! See line 7

Of DIRECT listing and direction of max spread output.

SPOT-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

>QUIT

FINISH SPOT LINKED TO DIRECT-BACK TO DIRECT

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
ENGLISH, METRIC, PERCENT, DEGREES,
COMMENT, KEY, HELP, STATUS

>QUIT

FINISH DIRECT -- BACK TO FIRE1

QUIT all the way back to FIRE 1

FIRE1 KEYWORD?

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT,

MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS, QUIT

>MORTALITY

and run MORTALITY as an independent module.

```
MORTALITY KEYWORD?
```

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> INPUT

*(1) SCORCH HEIGHT, FT ? 1-200 OR QUIT >30

*(2) TREE HEIGHT, FT ? 20-200 >20,110,45

THE FOLLOWING VALUES WILL BE USED 20.0 65.0 110.0 OK ? Y-N

*(3) CROWN RATIO ? .1-1 > .8

(4) BARK THICKNESS OPTION ? 1-2
1-DETERMINE BY SPECIES AND DBH
2-DIRECT ENTRY

>1

(4) TREE SPECIES ? 1-5

1=WESTERN LARCH, DOUGLAS-FIR

2=WESTERN HEMLOCK

3=ENGELMANN SPRUCE, WESTERN RED CEDAR

4=LODGEPOLE PINE, SUBALPINE FIR

5=NONE OF THESE -

> 3

*(4) TREE DBH, IN ? 5-50

>5,25,10

THE FOLLOWING VALUES WILL BE USED

5.0 15.0 25.0

OK ? Y-N

>Y

MORTALITY KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>LIST

Bark thickness is the MORTALITY input. These are the options for getting the values in.

I here choices result in a prompt yor bark thickness -

or choose a species with sark thickness similar to the one you are interested in

MORTALITY

1--SCORCH HEIGHT, FT ----- 30.0 2--TREE HEIGHT, FT ----- 20.0 65.0 110.0 3--CROWN RATIO ------ .8

3--CROWN RATIO ----- .8
4--BARK THICKNESS, IN ---- .2 .4 .6

5.0 15.0 25.0

.2 .4 .6
3=ENGELMANN SPRUCE, WESTERN RED CEDAR

These values are
Calculated from
PARED CEDAR & Species and
DBH.

MORTALITY KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

DBH, IN

FROM: SPECIES

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG.

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> RUN

TABLE VARIABLE ? 0-2

O=NO MORE TABLES

1=MORTALITY LEVEL

2=CROWN VOLUME SCORCH

>1

MORTALITY LEVEL, %

(V4.0)

TREE I TREE DBH, IN

HEIGHT I

5.0 15.0 25.0

(FT)

20.0 T 100.

I

20.0 I 100.

65.0 I 90.

110.0 I 68. 46. 28.

I-----

Calculations are made for all input combinations specified. The user must determine which Combinations are unrealistic.

TABLE VARIABLE ? 0-2

O=NO MORE TABLES
1=MORTALITY LEVEL

2=CROWN VOLUME SCORCH

> 0

MORTALITY KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>QUIT

FINISH MORTALITY -- BACK TO FIRE1

```
FIRE1 KEYWORD?
```

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT,
MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM,
TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
ENGLISH, METRIC, PERCENT, DEGREES,
COMMENT, KEY, HELP, STATUS, QUIT

SCORCH independent

>SCORCH

SCORCH KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> INPUT

- *(1) AMBIENT AIR TEMPERATURE, F ? 33-120 OR QUIT >85
- *(2) FLAME LENGTH, FT ? .1-100
- *(3) MIDFLAME WINDSPEED, MI/H ? 0-99

SCORCH KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>LIST

SCORCH

1--AMBIENT AIR TEMP, F --- 85.0
2--FLAME LENGTH, FT ---- 8.0
3--MIDFLAME WINDSPEED, MI/H 5.0

SCORCH KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

> RUN

(VERSION 4.0)

CROWN SCORCH HEIGHT, FT

67.

```
SCORCH KEYWORD?
```

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

MORTALITY

>MORTALITY

MORTALITY-LINKED-TO-SCORCH KEYWORD?
ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> INPUT

*(2) TREE HEIGHT, FT ? 20-200 >20,110,45

THE FOLLOWING VALUES WILL BE USED 20.0 65.0 110.0 OK ? Y-N

. . .

*(3) CROWN RATIO ? .1-1

(4) BARK THICKNESS OPTION ? 1-2 1=DETERMINE BY SPECIES AND DBH 2=DIRECT ENTRY

> 2

(4) BARK THICKNESS, IN ? .1-5 > .2, .6, .2

THE FOLLOWING VALUES WILL BE USED
.2 .4 .6
OK ? Y-N

> Y

MORTALITY-LINKED-TO-SCORCH KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>LIST

MORTALITY-LINKED-TO-SCORCH

Mortality linked to scorch

Enter bark thickness directly this time.

This value has 57. Leen carried over yrom SCORCH. MORTALITY-LINKED-TO-SCORCH KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

> RUN

TABLE VARIABLE ? 0-2

O=NO MORE TABLES

1=MORTALITY LEVEL

2=CROWN VOLUME SCORCH

>1

MORTALITY LEVEL, % (V4.0) TREE I TREE DBH, IN HEIGHT I I 5.0 15.0 25.0 (FT) I-----20.0 I 99. 99. 98. I 99. 99. 98. 65.0 I I 110.0 I 97. 94. 88.

TABLE VARIABLE ? 0-2

0=NO MORE TABLES 1=MORTALITY LEVEL 2=CROWN VOLUME SCORCH

>0

MORTALITY-LINKED-TO-SCORCH KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

>QUIT

FINISH MORTALITY LINKED TO SCORCH--BACK TO SCORCH

SCORCH KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

MORTALITY

>QUIT

FINISH SCORCH - BACK TO FIRE1

```
FIRE1 KEYWORD?
```

ENTER DIRECT.SITE.SIZE.CONTAIN.SCORCH.SPOT.

MORTALITY.MAP.SLOPE.DISPATCH.CUSTOM.

TERSE.WORDY.PAUSE.NOPAUSE.LOG.NOLOG.

ENGLISH.METRIC.PERCENT.DEGREES.

COMMENT.KEY.HELP.STATUS.QUIT

DIRECT-SCORCH-MORTALITY Linked run

> DIRECT

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> INPUT

- (1) FUEL MODEL ? 0-99 OR QUIT

 (ENTER 0 FOR TWO FUEL MODEL CONCEPT INPUT.)
 >10
- *(2) 1-HR FUEL MOISTURE, % ? 1-60 >5,11,2

THE FOLLOWING VALUES WILL BE USED 5.0 7.0 9.0 11.0 OK ? Y-N

- *(3) 10-HR FUEL MOISTURE, % ? 1-60
- *(4) 100-HR FUEL MOISTURE, % ? 1-60
- *(6) LIVE WOODY MOISTURE, % ? 30-300 > 150
- *(7) MIDFLAME WINDSPEED, MI/H ? 0-99 >4,14,2

THE FOLLOWING VALUES WILL BE USED

4.0 6.0 8.0 10.0 12.0 14.0

OK ? Y-N

>Y

- *(8) TERRAIN SLOPE, % ? 0-100 >15
- *(9) DIRECTION OF WIND VECTOR,

 DEGREES CLOCKWISE FROM UPHILL ? 0-360

```
(10) DO YOU WANT FIRE BEHAVIOR PREDICTIONS FOR
      THE DIRECTION OF MAXIMUM SPREAD ? Y-N
 DIRECT KEYWORD?
 ENTER INPUT, LIST, CHANGE, RUN, QUIT,
      TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
       ENGLISH, METRIC, PERCENT, DEGREES,
      COMMENT, KEY, HELP, STATUS
>LIST
DIRECT
 1--FUEL MODEL ------ 10 -- TIMBER (LITTER AND UNDERSTORY)
 2--1-HR FUEL MOISTURE, % -- 5.0 7.0 9.0 11.0
 3--10-HR FUEL MOISTURE, % -
                              7.0
 4--100-HR FUEL MOISTURE, %
                               8.0
 6--LIVE WOODY MOISTURE, % - 150.0
 7--MIDFLAME WINDSPEED, MI/H 4.0 6.0 8.0 10.0 12.0 14.0
 8--TERRAIN SLOPE, % ----- 15.0
 9--DIRECTION OF WIND VECTOR .O
     DEGREES CLOCKWISE
      FROM UPHILL
 10--DIRECTION OF SPREAD ---- .O (DIRECTION OF MAX SPREAD)
    CALCULATIONS
     DEGREES CLOCKWISE
      FROM UPHILL
DIRECT KEYWORD?
ENTER INPUT, LIST, CHANGE, RUN, QUIT,
      TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
      ENGLISH, METRIC, PERCENT, DEGREES,
      COMMENT, KEY, HELP, STATUS
> RUN
```

TABLE VARIABLE ? 0-6

0=NO MORE TABLES 4=FLAME LENGTH 1=RATE OF SPREAD 5=REACTION INTENSITY 2=HEAT PER UNIT AREA 6=EFFECTIVE WINDSPEED

3=FIRELINE INTENSITY

>4

FLAME LENGTH, FT (V4.0)

-----1-HR I MIDFLAME WIND, MI/H MOIS I 4.0 6.0 8.0 10.0 12.0 14.0 (%) 7.9 5.0 I 4.1 5.2 6.1 7.0 8.7 I 7.0 I 3.8 4.8 5.7 6.6 7.4 8.2 9.0 I 3.7 4.6 5.5 6.3 7.1 7.8 11.0 I 3.6 4.5 5.3 6.1 6.9 7.6

TABLE VARIABLE ? 0-6

O=NO MORE TABLES 4=FLAME LENGTH

1=RATE OF SPREAD 5=REACTION INTENSITY

2=HEAT PER UNIT AREA 6=EFFECTIVE WINDSPEED

3=FIRELINE INTENSITY

> 0

IF YOU WANT TO CONTINUE WITH THE AREA AND PERIMETER CALCULATIONS, TYPE 'SIZE'

IF YOU WANT TO CONTINUE WITH SCORCH HEIGHT CALCULATIONS,

TYPE 'SCORCH'

IF YOU WANT TO CONTINUE WITH SPOTTING DISTANCE FROM A WIND-DRIVEN SURFACE FIRE, TYPE 'SPOT'

DIRECT KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

SIZE,SCORCH,SPOT

SCORCH

SCORCH-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

> INPUT

*(1) AMBIENT AIR TEMPERATURE, F ? 33-120 OR QUIT > 75

The only SCORCH input in a linked run.

SCORCH-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

>LIST

These values are Carried over grom DIRECT.

SCORCH-LINKED-TO-DIRECT

1--AMBIENT AIR TEMP, F ---- 75.0

2--FLAME LENGTH, FT ----- OUTPUT FROM DIRECT. RANGE = 3.6 TO 8.7 3--MIDFLAME WINDSPEED, MI/H - SAVED FROM DIRECT. RANGE = 4.0 TO 14.0

SCORCH-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

> RUN

CROWN SCORCH HEIGHT, FT ______ 1-HR I MIDFLAME WIND, MI/H MOIS I 8.0 10.0 12.0 14.0 I 4.0 6.0 (%) I------Ī 19. 29. 5.0 I 23. 26. 28. 31. I 17. 20. 22. 24. 7.0 I 25. 26. Т 9.0 I 22. 23. 16. 18. 20. 15. 20. 21. 22. 11.0 I 17. 19.

SCORCH-LINKED-TO-DIRECT KEYWORD? ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

MORTALITY

>MORTALITY

MORTALITY-LINKED-TO-DIRECT-AND-SCORCH KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

>INPUT

```
*(2) TREE HEIGHT, FT ? 20-200
>50
*(3) CROWN RATIO ? .1-1
> . 6
(4) BARK THICKNESS OPTION ? 1-2
      1=DETERMINE BY SPECIES AND DBH
      2=DIRECT ENTRY
>2
*(4) BARK THICKNESS, IN ? .1-5
>.1
MORTALITY-LINKED-TO-DIRECT-AND-SCORCH KEYWORD?
ENTER INPUT.LIST.CHANGE.RUN.OUIT.
      TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
      ENGLISH, METRIC, PERCENT, DEGREES,
      COMMENT, KEY, HELP, STATUS
>LIST
MORTALITY-LINKED-TO-DIRECT-AND-SCORCH
 1--SCORCH HEIGHT, FT ----- OUTPUT FROM SCORCH, RANGE = 15. TO 31.
  2--TREE HEIGHT, FT ----- 50.0
 3--CROWN RATIO ----- .6
 4--BARK THICKNESS, IN ----
                                 . 1
       (DIRECT ENTRY)
 MORTALITY-LINKED-TO-DIRECT-AND-SCORCH KEYWORD?
 ENTER INPUT, LIST, CHANGE, RUN, QUIT,
      TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
      ENGLISH, METRIC, PERCENT, DEGREES,
      COMMENT, KEY, HELP, STATUS
> RUN
 TABLE VARIABLE ? 0-2
  O=NO MORE TABLES
  1=MORTALITY LEVEL
   2=CROWN VOLUME SCORCH
>1
```

MORTALITY LEVEL. % MIDFLAME WIND, MI/H 1-HR I MOIS I I 4.0 6.0 8.0 10.0 12.0 14.0 (%) 5.0 73. 77. 84. 89. 92. I 94. I 73. 73. 75. 79. 82. 7.0 85. I 73. 73. 73. 74. 9.0 I 76. 78. I 11.0 I 73. 73. 73. 73. 74. 75.

TABLE VARIABLE ? 0-2

0=NO MORE TABLES

1=MORTALITY LEVEL

2=CROWN VOLUME SCORCH

>0

MORTALITY-LINKED-TO-DIRECT-AND-SCORCH KEYWORD?
ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

>QUIT

FINISH MORTALITY LINKED TO SCORCH AND DIRECT--BACK TO SCORCH

SCORCH-LINKED-TO-DIRECT KEYWORD?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY,HELP,STATUS

MORTALITY

>QUIT

FINISH SCORCH - BACK TO DIRECT

DIRECT KEYWORD?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS

SIZE, SCORCH, SPOT

>QUIT

FINISH DIRECT -- BACK TO FIRE1

FIRE1 KEYWORD?

ENTER DIRECT, SITE, SIZE, CONTAIN, SCORCH, SPOT,

MORTALITY, MAP, SLOPE, DISPATCH, CUSTOM,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS, QUIT

>QUIT

DO YOU REALLY WANT TO TERMINATE THIS RUN? Y-N

PART OF THIS RUN MAY HAVE BEEN LOGGED.
THE FILE NAME IS: LOGFIL
PRINT THE FILE NOW AND DELETE IT.

FIRE1 RUN TERMINATED.

A reminder of your log yile name and incouragement to delete it when you no longer need it. you are responsible for your own file maintenance. WELCOME TO THE BEHAVE SYSTEM

BURN SUBSYSTEM

FIRE2 PROGRAM: VERSION 4.0 -- MAY 1989

DEVELOPED BY: THE FIRE BEHAVIOR RESEARCH WORK UNIT
INTERMOUNTAIN FIRE SCIENCES LABORATORY
MISSOULA, MONTANA

YOU ARE RESPONSIBLE FOR SUPPLYING VALID INPUT AND FOR CORRECTLY INTERPRETING THE FIRE BEHAVIOR PREDICTIONS.

ASSUMPTIONS, LIMITATIONS, AND APPLICATION OF MATHEMATICAL
MODELS USED IN THIS PROGRAM ARE IN:
Andrews, Patricia L. "BEHAVE: Fire behavior prediction and
fuel modeling system--BURN subsystem, Part 1", INT-GTR-194, 1986.
Andrews, Patricia L., and Chase, Carolyn H. "BEHAVE: Fire
behavior prediction and fuel modeling system--BURN
subsystem, Part 2", INT-GTR-260, 1989.

(PRESS RETURN TO CONTINUE)

PAUSE OPTION AND ENGLISH UNITS SET.

SLOPE MEASUREMENT IS IN PERCENT.

WHEN YOU ARE READY TO CONTINUE AFTER THE PROMPT SYMBOL IS
PRINTED WITHOUT A QUESTION, PRESS THE CARRIAGE RETURN KEY.

TYPE 'CUSTOM' IF YOU ARE GOING TO USE CUSTOM FUEL MODELS.

FIRE2 KEYWORD ?

ENTER IGNITE, MOISTURE, RH, CUSTOM,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY, HELP, STATUS, QUIT

>LOG

WHAT FILE NAME DO YOU WANT TO USE? (12 CHARACTERS MAX)
FIRST CHARACTER MUST BE ALPHABETIC. FOLLOW THE NAMING
CONVENTION FOR YOUR COMPUTER.

>LOGFIL

LOG FILE "LOGFIL" EXISTS. DO YOU WANT TO

1=APPEND TO FILE "LOGFIL"

2=CHANGE TO ANOTHER LOG FILE

3=DELETE "LOGFIL" AND START A NEW FILE WITH THE SAME NAME

LOG IS ON.

THE NAME OF YOUR LOGFILE IS: LOGFIL

He used this file for the FIRE I run and did not delete. You must make a Choice.

FIRE2 KEYWORD ? ENTER IGNITE, MOISTURE, RH, CUSTOM. TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG. ENGLISH, METRIC, PERCENT, DEGREES, COMMENT, KEY, HELP, STATUS, QUIT MOISTURE MOISTURE KEYWORD ? ENTER INPUT, LIST, CHANGE, RUN, QUIT, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH. METRIC. PERCENT. DEGREES. COMMENT, KEY HELP, STATUS > INPUT REMINDER: 'BURN DAY' STARTS AT NOON AND CONTINUES FOR 24 HOURS. ALL INPUTS ARE IN REFERENCE TO 'BURN DAY.' (1) RUN OPTION ? 1-2 OR QUIT 1 = BURN TIME CALCULATIONS 2 = HOURLY CALCULATIONS (GRAPHIC OUTPUT) > 2 (2) MONTH OF BURN ? 1-12

Graphic option

>7

(3) DAY OF BURN ? 1-31

(4) LATITUDE, DEG. ? O TO 90

(4) NORTH OR SOUTH OF THE EQUATOR ? N-S > N

SUNSET = 1926.

(5) BURN TIME ? 0000-2359

>10

(12) ELEVATION OF FIRE LOCATION, FT ? 0 TO 12000

> Y

>1000

dine I is used in MOISTURE but not in SITE.

Lines 7-10 are used in SITE Just not in MOISTURE.

There is no latitude estimation by state abbreviation in MOISTURE. MOISTURE and SITE can now handle southern latitudes.

(To obtain a 24-hour diversal prediction, you must use a turn time of 1100 to 1159 (because of the definition of ourn day).

(No 2-juil-model concept is allowed in MOISTURE.

Ful models are used only to provide a fuel depth
for wind adjustment purposes. Custom full models
are allowed. Shere are no slope helps in MOISTURE Las there are in SITE.

(12) ELEVATION OF FIRE LOCATION. FT? 0 TO 12000

(13) ARE WEATHER OBSERVATIONS AT THE SAME ELEVATION

AS THE FIRE? Y-N

AS THE FIRE? Y-N

AND ISTURE.

- (14) ASPECT ? N,NE,E,SE,S,SW,W,NW
- (15) CROWN CLOSURE, % ? 0-100 OR QUIT (ENTER THE CLOSURE AS IF THERE WERE FOLIAGE)
- (22) BURN DAY 1400 TEMPERATURE, F ? 33 TO 120 OR QUIT >85
- (23) BURN DAY 1400 RELATIVE HUMIDITY, % ? 1 TO 100 >20
- (24) BURN DAY 1400 20-FOOT WINDSPEED, MI/H ? 0 TO 99
- (25) BURN DAY 1400 CLOUD COVER, % ? 0 TO 100
- (26) BURN DAY 1400 HAZINESS ? 1-4

 1=VERY CLEAR SKY

 2=AVERAGE CLEAR FOREST ATMOSPHERE

 3=MODERATE FOREST BLUE HAZE

 4=DENSE HAZE

(27) SUNSET TEMPERATURE, F ? 33 TO 120

>1

- (28) SUNSET RELATIVE HUMIDITY, % ? 1 TO 100
- (29) SUNSET 20-FOOT WINDSPEED, MI/H ? 0 TO 99
- (30) SUNSET CLOUD COVER, % ? 0 TO 100
- (31) SUNRISE TEMPERATURE, F ? 33 TO 120
- (32) SUNRISE RELATIVE HUMIDITY, % ? 1 TO 100 >35
- (33) SUNRISE 20-FOOT WINDSPEED, MI/H ? 0 TO 99
- (34) SUNRISE CLOUD COVER, % ? 0 TO 100
- (35) BURN TIME TEMPERATURE, F ? 33 TO 120

There is no estimation of relative humidity for sunset, survise, burn time in MOISTURE (this capability is still available in SITE).

(36) BURN TIME RELATIVE HUMIDITY, % ? 1 TO 100 >30 (37) BURN TIME 20-FOOT WINDSPEED, MI/H ? O TO 99 (38) BURN TIME CLOUD COVER, % ? O TO 100 (39) BURN TIME HAZINESS ? 1-4 1=VERY CLEAR SKY 2=AVERAGE CLEAR FOREST ATMOSPHERE 3=MODERATE FOREST BLUE HAZE 4 = DENSE HAZE >1 In MOISTURE, there is no help in determining exposure to wind as there is in SITE.

Option 5 is new to SITE. (40) EXPOSURE TO WIND ? 1-5 1 = EXPOSED 2 = PARTIALLY SHELTERED 3 = FULLY SHELTERED -- OPEN STAND 4 = FULLY SHELTERED -- DENSE STAND 5 = DIRECT ENTRY OF WIND ADJUSTMENT FACTOR > 1 (43) MOISTURE INITIALIZATION OPTION ? 1-5 OR QUIT 1=1-HR FUEL MOISTURE KNOWN FOR BURN DAY -1 2=COMPLETE WEATHER DATA FOR 3 TO 7 DAYS 3=INCOMPLETE WEATHER DATA RAIN THE WEEK BEFORE THE BURN 4=INCOMPLETE WEATHER DATA NO RAIN THE WEEK BEFORE THE BURN WEATHER PATTERN HOLDING (NO ADDITIONAL INPUT) 5=INCOMPLETE WEATHER DATA WEATHER PATTERN CHANGING > 3 (51) NUMBER OF DAYS BEFORE THE BURN THAT RAIN OCCURRED ? 1-7 Precipitation amounts can be put in to the nearest hundredth (both 5 ITE (52) RAIN AMOUNT, (INCHES)? .01 TO 4 and MOISTURE). SITE (English) unitso INED, F? 33 TO 120 for this insput have tun Changed to inches. (53) 1400 TEMPERATURE ON THE DAY IT RAINED, F ? 33 TO 120 >70

```
(54) SKY CONDITION FROM THE DAY IT RAINED TIL BURN DAY ? 1-3
     1=CLEAR
     2=CLOUDY
     3=PARTLY CLOUDY
>1
MOISTURE KEYWORD ?
ENTER INPUT, LIST, CHANGE, RUN, QUIT,
     TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
      ENGLISH, METRIC, PERCENT, DEGREES,
      COMMENT, KEY HELP, STATUS
>LIST
MOISTURE
 1--RUN OPTION------ 2=HOURLY CALCULATIONS (GRAPHIC OUTPUT)
 2--MONTH OF BURN----- 7.
 3--DAY OF BURN----- 25.
 4--LATITUDE----- 46. N
 5--BURN TIME (2400 HOURS)-- 1150.
                           433. = TIME OF SUNRISE
                          1926.=TIME OF SUNSET
 6--FUEL MODEL
                             5 = BRUSH (2 FT)
11--TERRAIN SLOPE, % ----- 10.0
12--ELEVATION OF FIRE
     LOCATION, FT ----- 1000.0
13--ELEVATION OF WEATHER
     OBSERVATIONS, FT---- SAME AS FIRE LOCATION
14--ASPECT-----
                             .0
15--CROWN CLOSURE, % -----
22--BURN DAY 1400 TEMP, F -- 85.0
23--BURN DAY 1400 RH, % ---- 20.0
24--BURN DAY 1400 20-FOOT
     WIND SPEED, MI/H -----
                           5.0
25--BURN DAY 1400 CLOUD
     COVER, % -----
                              . 0
26--BURN DAY 1400 HAZINESS-- 1=VERY CLEAR SKY
27--SUNSET TEMPERATURE, F -- 68.0
28--SUNSET RH, % -----
                           30.0
29--SUNSET 20-FOOT
    WIND SPEED, MI/H -----
                             .0
```

. 0

30--SUNSET CLOUD COVER, % --

31SUNRISE TEMPERATURE, F -	57.0
32SUNRISE RH, %	35.0
29SUNRISE 20-FOOT	
WIND SPEED, MI/H	.0
34SUNRISE CLOUD COVER, % -	.0
35BURN TIME TEMPERATURE, F	70.0
36BURN TIME RH, %	30.0
37BURN TIME 20-FOOT	
WIND SPEED, MI/H	5.0
38BURN TIME CLOUD COVER, %	.0
39BURN TIME HAZINESS	1=VERY CLEAR SKY
40EXPOSURE OF FUELS TO	
THE WIND	1=EXPOSED
	.4=WIND ADJUSTMENT FACTOR
>	
43MOISTURE INITIALIZATION	
CODE	3=INCOMPLETE WEATHER DATA
	RAIN THE WEEK BEFORE THE BURN
51NUMBER OF DAYS BEFORE	
BURN THAT RAIN OCCURRED	5.0
52RAIN AMOUNT, INCHES	.09
531400 TEMPERATURE ON	
THE DAY IT RAINED, F	70.0
54SKY CONDITION AFTER THE	
DAY IT RAINED	1 = CLEAR
MOISTURE KEYWORD ?	
ENTER INPUT, LIST, CHANGE, RUN, Q	UIT,
TERSE, WORDY, PAUSE, NOPAU	OR LOG WOLGS
	SE, LOG, NOLOG,
ENGLISH, METRIC, PERCENT,	
ENGLISH, METRIC, PERCENT, COMMENT, KEY HELP, STATUS	

> RUN

PLOT VARIABLE ? 0-11

O=NO MORE GRAPHS

1=1-HR FUEL MOISTURE

2=DRY BULB TEMPERATURE

3=AIR RH

4=FUEL LEVEL TEMPERATURE

5=FUEL LEVEL RH

11=2 OR MORE PARAMETERS

ON SAME AXES

Jabular output provides the values of all 9 parameters (1-9) each hour from noon until burn time.

(VERSI	ON 4.0)	1								
LOCAL	1-HR	DRY	AIR	FUEL	FUEL	MID-	FUEL	SHADE	PROB)
SUN	FUEL	BULB	RH	LEVEL	LEVEL	FLAME	LEVEL		OF	10
TIME	MOIS	TEMP		TEMP	RH	WIND	WIND		IGN	Probability of
(HR)	(%)	(F)	(%)	(F)	(%)	(MI/H)	(MI/H)	(%)	(%)	ignition in MOISTURE
1200	3.9	85.	20.	113.	8.	2.0	1.1	Ο.	80.	
1300	3.9	85.	20.	113.	8.	2.0	1.1	ο.	80.	uses the predicted
1400	3.9	85.	20.	113.	8.	2.0	1.1	ο.	80.	Yull level temperature
1500	3.2	84.	20.	108.	9.	1.6	. 9	ο.	80.	Distance and as incl
1600	3.1	82.	22.	101.	12.	1.3	. 7	0.	80.	in the prob. of ign.
1700	3.1	79.	24.	91.	16.	. 9	. 5	ο.	80.	equations instead of
1800	3.3	75.	26.	79.	23.	. 5	. 3	ο.	80.	0, , , ,
1900	3.6	70.	29.	70.	29.	. 2	. 1	Ο.	70.	the ful temperature
2000	3.9	67.	30.	67.	30.	.0	. 0	100.	70.	estimate based on
2100	4.1	65.	31.	65.	31.	.0	.0	100.	60.	
2200	4.4	63.	32.	63.	32.	.0	. 0	100.	60.	air temp and shade
2300	4.6	62.	33.	62.	33.	.0	.0	100.	60.	as in the prob. of.
2400	4.8	60.	34.	60.	34.	.0	. 0	100.	60.	im Tables the
100	5.1	59.	34.	59.	34.	.0	. 0	100.	50.	sign. parte. The
200	5.3	58.	35.	58.	35.	.0	. 0	100.	50.	result is rounded
300	5.6	57.	35.	57.	35.	.0	.0	100.	50.	to the nearest 10%.
400	5.8	57.	35.	57.	35.	.0	. 0	100.	50.	
)
										ζ
	ON 4.0									1 11 V ad i da
LOCAL	1-HR	DRY	AIR	FUEL	FUEL	MID-	FUEL	SHADE	PROB	The headings are
SUN	FUEL	BULB	RH	LEVEL	LEVEL	FLAME	LEVEL		OF	hespeated on the
TIME	MOIS	TEMP		TEMP	RH	WIND	WIND	40.3	IGN	the second
(HR)	(%)	(F)	(%)	(F)	(%)	(MI/H)		(%)	(%)	terminal for your
500	6.0	57.	35.	57.	35.	. 1	.1	0.	50.	Convenience They
600	6.2	58.	35.	66.	27.	. 4	. 2	0.	50.	Ola Amittade in
700	6.2	59.	34.	76.	20.	.7	. 4	0.	50.	are omitted in
800	5.9	60.	34.	85.	15.	.9	. 5	0.	50.	log files.
900	5.3	63.	33.	93.	12.	1.2	.7	0.	60.	00
1000	4.7	65.	32.	98.	11.	1.5	. 9	0.	70.	
1100	4.0	68.	31.	101.	10.	1.8	1.0	Ο.	70.	

PLOT VARIABLE ? 0-11

4.0

70.

O=NO MORE GRAPHS 6=MIDFLAME WIND
1=1-HR FUEL MOISTURE 7=FUEL LEVEL WIND

2=DRY BULB TEMPERATURE 8=SHADE PERCENT

3=AIR RH

>1

>1

1150

4=FUEL LEVEL TEMPERATURE 10=TABULAR OUTPUT

5=FUEL LEVEL RH

9=PROBABILITY OF IGNITION

30. 103. 10. 2.0 1.1 0.

11=2 OR MORE PARAMETERS

ON SAME AXES

SCALE OPTION ? 1-2

1 = USE THE CALCULATED Y-AXIS RANGE

2 = SET THE Y-AXIS RANGE

The calculated y-axis range spreads the plot vertically as much as possible.

70.

Parameter being plotted 1-HR FUEL MOISTURE, % 1 1 1 6-1 I corresponds to the list number from above for this parameter 1 5.5-. 5-! 1 4.5-! 4-111 1 3.5-3--!--!--!--!--!--!--!--!--!--! 12 14 16 18 20 22 24 2 4 6 8 10 12 5 = sunset R = sunrise LOCAL SUN TIME (HOUR) PLOT VARIABLE ? 0-11 0=NO MORE GRAPHS 6=MIDFLAME WIND 1=1-HR FUEL MOISTURE 7=FUEL LEVEL WIND 2=DRY BULB TEMPERATURE 8=SHADE PERCENT 3=AIR RH 9=PROBABILITY OF IGNITION 4=FUEL LEVEL TEMPERATURE 10=TABULAR OUTPUT More than 2 or 3 becomes too busy to be useful. 5=FUEL LEVEL RH 11=2 OR MORE PARAMETERS ON SAME AXES >11 PARAMETER NO. 1? 0=NO MORE PARAMETERS 5=FUEL LEVEL RH 1=1-HR FUEL MOISTURE 6=MIDFLAME WIND 2=DRY BULB TEMPERATURE 7=FUEL LEVEL WIND 3=AIR RH 8=SHADE PERCENT 4 = FUEL LEVEL TEMPERATURE 9 = PROBABILITY OF IGNITION > 2 PARAMETER NO. 2? 0=NO MORE PARAMETERS 5=FUEL LEVEL RH 1=1-HR FUEL MOISTURE 6=MIDFLAME WIND 2=DRY BULB TEMPERATURE 7=FUEL LEVEL WIND 3=AIR RH 8=SHADE PERCENT 4=FUEL LEVEL TEMPERATURE 9=PROBABILITY OF IGNITION

>4

PARAMETER NO. 3? O=NO MORE PARAMETERS 5=FUEL LEVEL RH 1=1-HR FUEL MOISTURE 6=MIDFLAME WIND 2=DRY BULB TEMPERATURE 7=FUEL LEVEL WIND 3=AIR RH 8=SHADE PERCENT 4=FUEL LEVEL TEMPERATURE 9=PROBABILITY OF IGNITION SCALE OPTION ? 1-2 1 = USE THE CALCULATED Y-AXIS RANGE 2 = SET THE Y-AXIS RANGE >2 Let's set our own y-axis range this time. Y-AXIS MINIMUM ? 0-200 Y-AXIS MAXIMUM ? 0-200 >115 1=1-HR 2=DBULB 3=RH 4 = FTEMP 5=FRH 6=MWIND 7=FWIND 8=SHADE 9=P 120-

The key to the plotted parameters corresponds to the list

Imagine the smooth Curve sketched in. The steps in the line are due to the resolution of the character

Fuel temperature (4) plotted on top of air temperature here, so the 2's disappeared.

1 110-100-90-1 2 2 2 2 80-70-60-12 14 16 18 20 22 24 8 10 12 S LOCAL SUN TIME (HOUR)

PLOT VARIABLE ? 0-11

0=NO MORE GRAPHS 1=1-HR FUEL MOISTURE 2=DRY BULB TEMPERATURE

4=FUEL LEVEL TEMPERATURE 10=TABULAR OUTPUT 5=FUEL LEVEL RH

6=MIDFLAME WIND 7=FUEL LEVEL WIND 8=SHADE PERCENT

9=PROBABILITY OF IGNITION

11=2 OR MORE PARAMETERS ON SAME AXES

> 0

VERSION 4.0

```
MOISTURE KEYWORD ?
 ENTER INPUT, LIST, CHANGE, RUN, QUIT,
       TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
       ENGLISH, METRIC, PERCENT, DEGREES,
       COMMENT, KEY HELP, STATUS
> INPUT
 REMINDER: 'BURN DAY' STARTS AT NOON AND CONTINUES FOR 24
            HOURS. ALL INPUTS ARE IN REFERENCE TO 'BURN DAY.'
                                                Run option must be I for ranging insput to be acceptable. It waing CHANGE, be sure to change line I
 (1) RUN OPTION ? 1-2 OR QUIT
    1 = BURN TIME CALCULATIONS
     2 = HOURLY CALCULATIONS (GRAPHIC OUTPUT)
> 1
(2) MONTH OF BURN ? 1-12
 (3) DAY OF BURN ? 1-31
>30
(4) LATITUDE, DEG. ? O TO 90
>40
 (4) NORTH OR SOUTH OF THE EQUATOR ? N-S
> N
SUNSET = 1918.
SUNRISE = 442.
 (5) BURN TIME ? 0000-2359
>1500
(6) FUEL MODEL ? 1-99
                                                    Note the * to indicate
> 2
                                                    which lines allow ranges
*(11) TERRAIN SLOPE, % ? 0 TO 100
                                                   yor option. The star did
unot appear in the last run
*(12) ELEVATION OF FIRE LOCATION, FT ? 0 TO 12000
                                                    when run option = 2.
>4500
 (13) ARE WEATHER OBSERVATIONS AT THE SAME ELEVATION
       AS THE FIRE ? Y-N
                                                             The choice is all or only one.
(14) DO YOU WANT CALCULATIONS FOR ALL ASPECTS ? Y-N
(15) CROWN CLOSURE, % ? 0-100 OR QUIT
```

(ENTER THE CLOSURE AS IF THERE WERE FOLIAGE)

>10

Shade calculations have (16) IS FOLIAGE PRESENT ? Y-N > Y been adjusted to better account for (17) ARE THE TREES IN THE STAND SHADE TOLERANT? Y-N 1. broad, glat Crowns (18) DOMINANT TREE TYPE ? 1-2 I light stocking levels. In some cases this will result 1 = CONIFEROUS 2 = DECIDUOUS >1 *(19) AVERAGE TREE HEIGHT, FT ? 10 TO 300 predictions and different values of strade, fuel temp, *(20) RATIO OF CROWN LENGTH TO TREE HEIGHT ? .1-1 *(21) RATIO OF CROWN LENGTH TO CROWN DIAMETER ? ctions can be expected *(22) BURN DAY 1400 TEMPERATURE, F ? 33 TO 120 OR QUIT in these situations for >60.72.2 versions 3.3 and later THE FOLLOWING VALUES WILL BE USED - timber Cover at light 60.0 62.0 64.0 66.0 68.0 70.0 72.0 OK ? Y-N stocking levels broad, glat crowns > Y *(23) BURN DAY 1400 RELATIVE HUMIDITY, % ? 1 TO 100 *(24) BURN DAY 1400 20-FOOT WINDSPEED, MI/H ? 0 TO 99 > 5 *(25) BURN DAY 1400 CLOUD COVER, % ? 0 TO 100 >0 (26) BURN DAY 1400 HAZINESS ? 1-4 1=VERY CLEAR SKY 2=AVERAGE CLEAR FOREST ATMOSPHERE 3=MODERATE FOREST BLUE HAZE 4=DENSE HAZE >1 BURN TIME IS BETWEEN 1200 AND 1600. BURN TIME CONDITIONS WILL BE SET TO 1400 CONDITIONS (40) EXPOSURE TO WIND ? 1-5 1 = EXPOSED

>1

5 = DIRECT ENTRY OF WIND ADJUSTMENT FACTOR

2 = PARTIALLY SHELTERED

3 = FULLY SHELTERED--OPEN STAND 4 = FULLY SHELTERED--DENSE STAND

```
(43) MOISTURE INITIALIZATION OPTION ? 1-5 OR QUIT
      1=1-HR FUEL MOISTURE KNOWN FOR BURN DAY -1
      2=COMPLETE WEATHER DATA FOR 3 TO 7 DAYS
      3=INCOMPLETE WEATHER DATA
        RAIN THE WEEK BEFORE THE BURN
      4=INCOMPLETE WEATHER DATA
        NO RAIN THE WEEK BEFORE THE BURN
        WEATHER PATTERN HOLDING
        (NO ADDITIONAL INPUT)
      5=INCOMPLETE WEATHER DATA
        WEATHER PATTERN CHANGING
> 4
MOISTURE KEYWORD ?
ENTER INPUT, LIST, CHANGE, RUN, QUIT,
      TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
      ENGLISH, METRIC, PERCENT, DEGREES,
      COMMENT, KEY HELP, STATUS
>LIST
 MOISTURE
 1--RUN OPTION------ 1=BURN TIME CALCULATIONS
  2--MONTH OF BURN-----
                            5.
 3--DAY OF BURN-----
  4--LATITUDE----- 40. N
  5--BURN TIME (2400 HOURS)-- 1500.
                            442. = TIME OF SUNRISE
                           1918. = TIME OF SUNSET
                              2 = TIMBER (GRASS AND UNDERSTORY)
  6--FUEL MODEL
 11--TERRAIN SLOPE, % ----- 10.0
 12--ELEVATION OF FIRE
     LOCATION, FT ----- 4500.0
                                                    First ranging variable
 13--ELEVATION OF WEATHER
       OBSERVATIONS, FT----- SAME AS FIRE LOCATION
 14--ASPECT----- ALL ASPECTS
 15--CROWN CLOSURE, % ----- 10.0
 16--FOLIAGE-----
 17--SHADE TOLERANCE-----
                             INTOLERANT
                             1=CONIFEROUS
  18--DOMINANT TREE TYPE----
  19--AVERAGE TREE HEIGHT, FT 50.0
  20--RATIO OF CROWN LENGTH
      TO TREE HEIGHT-----
                               .7
  21--RATIO OF CROWN LENGTH
      TO CROWN DIAMETER----
                              3.0
```

22--BURN DAY 1400 TEMP, F -- 60.0 62.0 64.0 66.0 68.0 70.0 72.0

23--BURN DAY 1400 RH, % ---- 40.0

24--BURN DAY 1400 20-FOOT

WIND SPEED, MI/H ----- 5.0

second ranging variable

25--BURN DAY 1400 CLOUD

COVER, % ----- .0

26--BURN DAY 1400 HAZINESS-- 1=VERY CLEAR SKY

BURN TIME WEATHER = 1400 WEATHER

Ic'll refer to this later.

40--EXPOSURE OF FUELS TO

THE WIND----- 1=EX

1=EXPOSED

.4 = WIND ADJUSTMENT FACTOR

43--MOISTURE INITIALIZATION

CODE----- 4=INCOMPLETE WEATHER DATA

NO RAIN THE WEEK BEFORE THE BURN

WEATHER PATTERN HOLDING

MOISTURE KEYWORD ?

ENTER INPUT, LIST, CHANGE, RUN, QUIT,

TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

ENGLISH, METRIC, PERCENT, DEGREES,

COMMENT, KEY HELP, STATUS

> RUN

TABLE VARIABLE ? 0-9

O=NO MORE TABLES 5=FUEL LEVEL RH

1=1-HR FUEL MOISTURE 6=MIDFLAME WINDSPEED

2=DRY BULB TEMPERATURE 7=FUEL LEVEL WINDSPEED

3=AIR RH 8=SHADE PERCENT

4=FUEL LEVEL TEMPERATURE 9=PROBABILITY OF IGNITION

>1

1-HR FUEL	MOISTUR	RE, %						(V4.0)
	I	BUR	N TIME	TEMPERA	TURE, D	EG F		
	Ι.							
ASPECT	ı	60.	62.	64.	66.	68.	70.	72.
	1							
	1							
N	I	5.1	5.1	5.1	5.0	5.0	5.0	5.0
	I							
NE	1	5.3	5.3	5.2	5.2	5.2	5.2	5.1
	I							
E	I	5.2	5.1	5.1	5.1	5.1	5.0	5.0
	I	(
SE	I	5.1	5.1	5.0	5.0	5.0	5.0	5.0
	I							
s	I	4.9	4.9	4.9	4.8	4.8	4.8	4.8
	I	1						

This column
assumes a turn
time temperature
of 60° on each
aspect. Note
the expected
variation in 1- hr
moisture depending
on aspect.

The moisture is printed to the nearest tenth of a percent to show brends in variation. The nearest percent is close enough for all practical purposes.

TABLE VARIABLE ? 0-9

NW

I

I

O=NO MORE TABLES

1=1-HR FUEL MOISTURE

2=DRY BULB TEMPERATURE

3=AIR RH

4=FUEL LEVEL TEMPERATURE

5=FUEL LEVEL RH
6=MIDFLAME WINDSPEED
7=FUEL LEVEL WINDSPEED
8=SHADE PERCENT
9=PROBABILITY OF IGNITION

4.8

4.8

4.8

4.9

MOISTURE KEYWORD ?

ENTER INPUT,LIST,CHANGE,RUN,QUIT,

TERSE,WORDY,PAUSE,NOPAUSE,LOG,NOLOG,

ENGLISH,METRIC,PERCENT,DEGREES,

COMMENT,KEY HELP,STATUS

4.8

4.9

Let's try CHANGE for the next run.

> CHANGE

> 0

CHANGE WHICH LINE ? 0-59
(O MEANS NO MORE CHANGES)

(5) BURN TIME ? 0000-2359

SINCE YOU HAVE CHANGED BURN TIME, YOU MAY ALSO WANT TO CHANGE BURN TIME WEATHER (LINES 35 THROUGH 39)

```
CHANGE WHICH LINE ? 0-59
  (O MEANS NO MORE CHANGES)
MOISTURE KEYWORD ?
ENTER INPUT, LIST, CHANGE, RUN, QUIT,
     TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,
      ENGLISH, METRIC, PERCENT, DEGREES.
      COMMENT, KEY HELP, STATUS
>LIST
MOISTURE
 1--RUN OPTION----- 1=BURN TIME CALCULATIONS
 2--MONTH OF BURN-----
 3--DAY OF BURN----- 30.
 4--LATITUDE----- 40. N
 5--BURN TIME (2400 HOURS)-- 1800.
                            442. = TIME OF SUNRISE
                          1918. = TIME OF SUNSET
 6--FUEL MODEL
                             2 = TIMBER (GRASS AND UNDERSTORY)
11--TERRAIN SLOPE, % ----- 10.0
12--ELEVATION OF FIRE
     LOCATION, FT ----- 4500.0
13--ELEVATION OF WEATHER
     OBSERVATIONS, FT----- SAME AS FIRE LOCATION
14--ASPECT----- ALL ASPECTS
15--CROWN CLOSURE, % ----- 10.0
16--FOLIAGE-----
                            PRESENT
17--SHADE TOLERANCE----- INTOLERANT
18--DOMINANT TREE TYPE----- 1=CONIFEROUS
19 -- AVERAGE TREE HEIGHT, FT
                           50.0
 20--RATIO OF CROWN LENGTH
     TO TREE HEIGHT-----
                              . 7
 21--RATIO OF CROWN LENGTH
     TO CROWN DIAMETER----
                            3.0
 22--BURN DAY 1400 TEMP, F -- 60.0 62.0 64.0 66.0 68.0 70.0 72.0
 23--BURN DAY 1400 RH, % ----
                            40.0
 24--BURN DAY 1400 20-FOOT
                            5.0
     WIND SPEED, MI/H -----
 25--BURN DAY 1400 CLOUD
```

. 0

1=VERY CLEAR SKY

 35--BURN TIME TEMPERATURE, F 60.0 62.0 64.0 66.0 68.0 70.0 72.0 36--BURN TIME RH, % ----- 40.0 37--BURN TIME 20-FOOT WIND SPEED, MI/H -----5.0 38--BURN TIME CLOUD COVER, % . 0 40--EXPOSURE OF FUELS TO

THE WIND-----1=EXPOSED

.4=WIND ADJUSTMENT FACTOR

See the listing from the previous run. These values were reset

because of burn time 4=INCOMPLETE WEATHER DATA

NO RAIN THE WEEK BEFORE THE BURN Choice. Be careful WEATHER PATTERN HOLDING

when using CHANGE to ENTER INPUT, LIST, CHANGE, RUN, QUIT, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG,

set up you the Next rux. always check your losting to see if it is what you intended. (Now there are 3 ranging variables.)

COMMENT, KEY HELP, STATUS

MOISTURE KEYWORD ?

43--MOISTURE INITIALIZATION

CODE-----

QUIT

FINISH MOISTURE -- BACK TO FIRE2

FIRE2 KEYWORD ? ENTER IGNITE, MOISTURE, RH, CUSTOM, TERSE, WORDY, PAUSE, NOPAUSE, LOG, NOLOG, ENGLISH, METRIC, PERCENT, DEGREES, COMMENT, KEY, HELP, STATUS, QUIT

ENGLISH, METRIC, PERCENT, DEGREES,

QUIT

DO YOU REALLY WANT TO TERMINATE THIS RUN ? Y-N

PART OF THIS RUN MAY HAVE BEEN LOGGED. THE FILE NAME IS: LOGFIL PRINT THE FILE NOW AND DELETE IT.

FIRE2 RUN TERMINATED. ********

APPENDIX B: INPUT/OUTPUT REFERENCE SHEETS

This appendix includes input/output reference sheets for all modules of the FIRE1 and FIRE2 programs of BE-HAVE. Some have the same items and line numbers as those given in Part 1 of this manual (DIRECT, SIZE, CONTAIN, DISPATCH), some are revised to reflect the changes described in the body of this paper (SPOT, SITE), and others are for new modules (SCORCH, MORTALITY, MAP, SLOPE, MOISTURE, IGNITE, RH). To avoid confusion with previous versions, a date is given at the bottom of each sheet.

The information on each sheet includes the item name, line number (as used by the CHANGE command), an * to indicate that a range of values is allowed, English and metric units, and comments. Only one blank is given for each input and output value. These are reference sheets rather than worksheets. A person will normally use a computer printout as a record of a run rather than writing the results on a worksheet. This is especially the case when a range of values is entered for two input values and the resulting output is a series of 7 x 7 tables.

These input/output sheets are alphabetized by module name. Refer to figure 3 for the relationship among the modules.

CONTAIN Module Input/Output (FIRE1 program)

		UNI	TS		COMMENTS
INPUT		English	Metric		
1	Mode of attack 1 = Head 2 = Rear				Direct attack
2	Run option 1 = Compute line building rate 2 = Compute burned area				
*3	Forward rate of spread	ch/h	m/min	—)	
*4	Initial fire size	ac	ha	}	May come from SIZE linked to DIRECT
*5	Length-to-width ratio)	inited to Birtheor
*6	Burned area target	ac	ha		If line building rate is computed
*7	Total line building rate	ch/h	m/min		If burned area is computed
					Total line building rate is twice the rate per flank
OUTPU	JT				
1	Total length of line	ch	m		Perimeter of burned area
2	Total containment time	h	h		
3 or	Total line building rate	ch/h	m/min		
3	Final fire size	ac	ha		

*A range of inputs is allowed

DIRECT Module Input/Output (FIRE1 program)

		UNI			COMMENTS
INPUT		English	Metric		
1	Fuel model				Enter 0 for two-fuel-model concept input
*2	1-h fuel moisture	%	%		
*3	10-h fuel moisture	%	%	— \	
*4	100-h fuel moisture	%	%	/	
*5	Live herbaceous fuel moisture	%	%	- \	If the fuel model has this size class
*6	Live woody fuel moisture	%	%	<i>)</i>	
*7	Midflame windspeed	mi/h	km/h		
*8	Slope	% or deg	% or deg		Units set using keywords PERCENT and DEGREES
*9	Direction of wind vector, deg clock-wise from uphill	deg	deg		If windspeed is not zero. Direction that the wind is pushing the fire
*10	Direction for spread calculations, deg clockwise from uphill (or from the wind vector if slope is zero)	deg	deg		Direction of maximum spread can be calculated
OUTPL	JT				
1	Rate of spread	ch/h	m/min		Fire behavior in the direction specified
2	Heat per unit area	Btu/ft ²	kJ/m²		in input line 10
3	Fireline intensity	Btu/ft/s	kW/m		
4	Flame length	ft	m		
5	Reaction intensity	Btu/ft²/min	kW/m²		
6	Effective windspeed	mi/h	k m /h		
7	Direction of maximum spread, deg clock-wise from uphill	deg	deg		
*A rang	ge of inputs is allowed				

DISPATCH Module Input/Output (FIRE1 program)

		UN English	ITS Metric		COMMENTS
INPUT		ŭ			
1	Fuel model				
2	Dead fuel moisture	%	%		1-h, 10-h, and 100-h
3	Live fuel moisture	%	%		Woody and herbaceous
4	20-foot windspeed	mi/h	km/h		Upslope wind
5	Wind adjustment factor				Midflame wind is 20-ft wind times wind adj. factor
6	Slope	% or deg	% or deg		wind times wind adj. ractor
7	Elapsed time from ignition to attack	h	h		
8	Total line building rate	ch/h	m/min		Twice the rate per flank
OUTPU	JT				
	Forward rate of spread	ch/h	m/min		
	Heat per unit area	Btu/ft²	kJ/m²		
	Fireline intensity	Btu/ft/s	kW/m		
	Flame length	ft	m		
	Perimeter at time of attack	ch	m		
	Area at time of attack	ac	ha		
He	ad attack: Elapsed time from attack to containment	h	h		
	Total length of line	ch	m		Perimeter of burned area
	Final fire size	ac	ha		
Re	ar attack: Elapsed time from attack to containment	h	h		
	Total length of line	ch	m		Perimeter of burned area
	Final fire size	ac	ha		

IGNITE Module Input/Output (FIRE2 program)

	UN	ITS	COMMENTS
	English	Metric	
INPUT			
*1 Dry bulb temperature	°F	°C	
*2 1-h fuel moisture	%	%	
*3 Shade	%	%	
ОИТРИТ			
Probability of ignition	%	%	
*A range of values is allowed.			

MAP Module Input/Output (FIRE1 program)

		UN	ITS		COMMENTS
		English	Metric		
INPUT					
1	Map scale	rep frac or in/mi	rep frac or cm/km		
2	Units option 1 = spread distance 2 = spot distance 3 = rate of spread				
*3	Spread distance	ch	m		If units option = 1
*4	Maximum spotting distance	mi	km		If units option = 2
*5	Rate of spread	ch/h	m/min)	If units option = 3
*6	Elapsed time	h	h	}	ii diilo option – o
OUTPU	JT				
or	Map spread distance	in	cm		If units option = 1, 3
Ol	Map maximum spotting distance	in	cm		If units option = 2
	distalice				In the direction of the wind

^{*}A range of values is allowed

MOISTURE Module Output (FIRE2 program)

(Use input sheets for SITE and MOISTURE combined)

		English	JNITS Metric	COMMENTS
1	1-h fuel moisture	%	%	
2	Dry bulb temperature	۰F	°C	
3	Air RH	%	%	
4	Fuel level temperature	· °F	°C	
5	Fuel level RH	%	%	
6	Midflame windspeed	mi/h	km/h	
7	Fuel level windspeed	mi/h	km/h	
8	Shade	%	%	
9	Probability of ignition	%	%	

MORTALITY Module Input/Output (FIRE1 program)

		1U	NITS		COMMENTS
		English	Metric		
INPUT					
*1	Scorch height	ft	m		May come from SCORCH
*2	Tree height	ft	m		
*3	Crown ratio				Ratio of crown length to tree height
*4	Bark thickness Direct input or from:	in	cm		to troe troight
	Species 1 = western larch, Douglas-fir 2 = western hemlock 3 = Engelmann spruce, western red cedar 4 = lodgepole pine, subalpine fir				
	DBH	in	cm		
OUTPU	JT				
1	Mortality level	%	%		
2	Crown volume scorch	%	%		

^{*} Range of values is allowed.

RH Module Input/Output (FIRE2 program)

	UN		COMMENTS	
INPUT	English	Metric		
*1 Dry bulb temperature	°F	°C	_	
*2 Wet bulb temperature	۰F	°C		
*3 Elevation	ft	m		
OUTPUT				
1 Relative humidity	%	%		
2 Dew point	°F	°C		

^{*} A range of values is allowed.

SCORCH Module Input/Output (FIRE1 program)

		UI	NITS		COMMENTS
INPUT		English	Metric		
*1	Ambient air temperature	۰F	°C		
*2	Flame length	ft	m	}	May come from DIRECT
*3	Midflame windspeed	mi/h	km/h	— }	may come non bineor
OUTP	JT				
	Crown scorch height	ft	m		

^{*} A range of values is allowed.

SITE and MOISTURE Module Input (SITE in FIRE1 program; MOISTURE in FIRE2 program)

	UI English	NITS Metric		COMMENTS
INPUT	Liigiioii	wethe		
 MOISTURE run option 1 = Burn time calculations 2 = Hourly calculations (graphic output) 			_	MOISTURE only
TIME AND LOCATION				
2 Month of burn				
3 Day of burn				
4 Latitude	deg	deg		
State				SITE only
5 Burn time (2400 hour)				If latitude is not known
FUEL MODEL				
6 Fuel model				
FUEL MOISTURE				
7 10-h fuel moisture	%	%	—)	
8 100-h fuel moisture	%	%	— (SITE only If this size class is
9 Live herbaceous moisture	%	%	— (in the fuel model
10 Live woody moisture	%	%	—)	
SLOPE, ELEVATION, ASPECT				
*11 Slope	% or deg	% or deg		Units set using keywords PERCENT or DEGREES
Map scale	rep frac or in/mi	rep frac or cm/km)	TENGENT OF DEGREES
Contour interval	ft	m	}	SITE only If slope is not known
Map distance	in	cm	\	ii siope is not known
Number of contour intervals			—)	
*12 Elevation of fire location	ft	m		

^{*} A range of values is allowed in MOISTURE only, run option 1.

		UN English	ITS Metric		COMMENTS
SLOPE	E, ELEVATION, ASPECT				
13	Elevation of T/RH obs.	ft	m		
*14	Aspect (N,NE,E,SE,S, SW,W,NW)				If slope is not zero
TIMBE	R OVERSTORY DESCRIPTION				
*15	Crown closure	%	%		
16	Foliage present or absent			—)	
17	Shade tolerant or intolerant)	
18	Dominant tree type 1 = Coniferous 2 = Deciduous			-	If crown closure is not zero
*19	Average tree height	ft	m	— (
*20	Ratio of crown length to tree height				
*21	Ratio of crown length to crown diameter			<i>— J</i>	
EARLY	AFTERNOON WEATHER				
*22	Burn day 1400 temperature	°F	°C		
*23	Burn day 1400 relative humidity	%	%	— /	Required input
*24	Burn day 1400 20-ft windspeed	mi/h	km/h	>	If burn time is between 1200 and 1600, 1400
*25	Burn day 1400 cloud cover	%	%		weather is used for burn time weather.
26	Burn day 1400 haziness 1 = very clear sky 2 = average clear forest atmosphere 3 = moderate forest blue haze 4 = dense haze or light to moderate smoke			<i> J</i>	

^{*} A range of values is allowed in MOISTURE only, run option 1.

		UNI ⁻ English	TS Metric	COMMENTS
SUNSE	T WEATHER	Liigiioii	Wow	
*27	Sunset temperature	°F	°C	\
*28	Sunset relative humidity	%	%	For burn time after sunset
*29	Sunset 20-ft windspeed	mi/h	km/h	and before 1200
*30	Sunset cloud cover	%	%	—) 12 16 33 Sh 12
SUNRIS	SE WEATHER			
*31	Sunrise temperature	°F	°C	—)
*32	Sunrise relative humidity	%	%	For burn time after sunrise
*33	Sunrise 20-ft windspeed	mi/h	km/h	and before 1200 12 16 SS SR 12
*34	Sunrise cloud cover	%	%	
BURN T	IME WEATHER			
*35	Burn time temperature	°F	°C	Ear burn time after 1600
	Burn time relative humidity	%	%	For burn time after 1600 or before 1200 12 16 SS SR 12
	Burn time 20-ft windspeed	mi/h	km/h	12 16 SS SR 12
	Burn time cloud cover	%	%	For burn time (after 1600 & before SS) or (after SR and before 1200)
39 (Burn time haziness 1 = very clear sky 2 = average clear forest atmosphere 3 = moderate forest blue haze 4 = dense haze or light to			12 16 SS SR 12 For burn time after sunrise and before 1200 12 16 SS SR 12

BURN TIME WIND

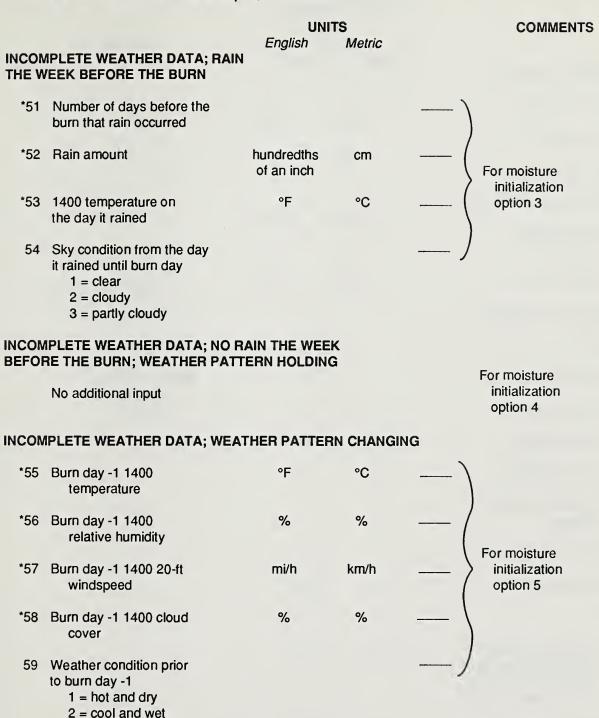
- 40 Exposure of fuels to the wind
 - 0 = Don't know (SITE only)

moderate smoke

- 1 = Exposed
- 2 = Partially sheltered
- 3 = Fully sheltered—open stand 4 = Fully sheltered—closed stand
- 5 = Direct entry of wind adjustment factor

^{*} A range of values is allowed in MOISTURE only, run option 1.

		_	•	NITS	Antrin		CC	OMMENTS
BURN	TIME WIND	<i>E1</i>	nglish	Λ.	1etric			
41	Burn time direction of wind vector degrees clockwise from uphi					 }	SITE	only
42	Direction for spread calculations degrees clockwise from uphi from wind vector if slope = 0 (direction of maximum sprea can be calculated)	il or				 }	0112	y
MOIST	URE INITIALIZATION OPTION							
43	Moisture initialization option 1 = Fine fuel moisture known the day before the burn 2 = Complete weather availab for 3 to 7 days prior to the 3 = Incomplete weather data a it rained the week before the beand weather pattern is star (no additional input) 5 = Incomplete weather data; weather pattern changing	burn ind he bur no urn,	n					
	UEL MOISTURE KNOWN HE DAY BEFORE THE BURN							
*44	Burn day -1 fine fuel moisture		%		%	 ı	or mois	sture initialization option 1
	LETE WEATHER AVAILABLE F DAYS PRIOR TO THE BURN	OR						
45	Number of days of weather	-1	-2	-3	-4	 -6	-7	
46						 		
47	Burn day -x 1400 relative humidity, %					 		. (
48	Burn day -x 1400 20-ft windspeed, mi/h or km/h					 		For moisture initialization option 2
49	Burn day -x 1400 cloud cover, %							
50	Burn day -x rain amount, hundredths of an inch or cm					 		
* A ran	ge of values is allowed in MOIST	URE	only, rur	n optio	n 1.			BEHAVE 1989



^{*}A range of values is allowed in MOISTURE only, run option 1.

3 =between 1 and 2

SITE Module Output (FIRE1 program)

		UN			COMMENTS
INTER	RMEDIATE VALUES	English	Metric		
	Time of sunset				
	Time of sunrise				
	Wind adjustment factor				
	Fuel surface temperature	°F	°C		
	Fuel level relative humidity	%	%		
	Percent shade	%	%		
	Fine dead fuel moisture	%	%		
BASIC	CINPUT				
	Fuel model				Corresponds to DIRECT input
	1-h fuel moisture	%	%		and output
	10-h fuel moisture	%	%		
	100-h fuel moisture	%	%		
	Live herbaceous fuel moisture	%	%		
	Live woody fuel moisture	%	%		
	Midflame windspeed	mi/h	km/h		
	Slope	%	%		
	Direction of wind vector, degrees clockwise from uphill (or from the wind vector if slope is zero)	deg	deg		
	Direction for spread calculations, degrees clockwise from uphill (or from the wind vector if slope is zero)	deg	deg		

SITE Module Output , continued:

	UNI	ITS		COMMENTS	
ОИТРИТ	English	Metric			
Rate of spread	ch/h	m/min			
Heat per unit area	Btu/ft²	kJ/m²			
Fireline intensity	Btu/ft/s	kW/m	_		
Flame length	ft	m			
Reaction intensity	Btu/ft²/min	kW/m²			
Effective windspeed	mi/h	km/h			
Direction of maximum spread, degrees clockwise from uphill	deg	deg			

MOISTURE Module Output (FIRE2 program)

	UN English	ITS Metric	COMMENTS	
1 1-h fuel moisture	%	%		
2 Dry bulb temperature	°F	°C		
3 Air RH	%	%		
4 Fuel level temperature	°F	°C		
5 Fuel level RH	%	%		
6 Midflame windspeed	mi/h	km/h		
7 Fuel level windspeed	mi/h	km/h		
8 Shade	%	%		
9 Probability of ignition	%	%	-	

SIZE Module Input/Output (FIRE1 program)

		UNI	TS	COMMENTS
		English	Metric	
INPUT				
*1	Rate of spread	ch/h	m/min	\ May come from DIRECT
*2	Effective windspeed	mi/h	km/h)
*3	Elapsed time	h	h	
OUTP	UT			
1	Area	ac	ha	
2	Perimeter	ch	m	
3	Length-to-width ratio			
4	Forward spread distance	ch	m	
5	Backing spread distance	ch	m	
6	Maximum width of fire	ch	m	

^{*}A range of values is allowed.

SLOPE Module Input/Output (FIRE1 program)

			ITS	COMMENTS
		English	Metric	
INPUT				
1	Map scale	rep frac or in/mi	rep frac or cm/km	 Can enter map scale either way
*2	Contour interval	ft	m	
*3	Map distance	in	cm	
*4	Number of contour intervals			
OUTP	UT			
1	Slope	% or deg	% or deg	 Units set using keywords PERCENT or DEGREES
2	Elevation change	ft	m	
3	Horizontal distance	ft	m	

^{*} A range of values is allowed.

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SPOT Module Input/Output (FIRE1 program)

		UNI	TS		COMMENTS
NOUT		English	Metric		
NPUT					
1	Firebrand source 1 = torching trees 2 = burning pile 3 = wind-driven surface fire				
*2	Mean cover height	ft	m	_	For torching trees or burning pile
*3	20-ft windspeed	mi/h	km/h		May come from DIRECT for wind-driven surface fire
*4	Ridge-to-valley elevation difference	ft	m	***************************************	
*5	Ridge-to-valley horizontal distance	mi	km	}	If ridge-to-valley
6	Spotting source location 0 = midslope, windward side 1 = valley bottom 2 = midslope, leeward side 3 = ridgetop)	If ridge-to-valley elevation difference is not equal to zero
7	Tree species 1 = Engelmann spruce 2 = Douglas-fir, subalpine fir 3 = hemlock 4 = ponderosa pine, lodgepole p 5 = white pine 6 = balsam fir, grand fir 7 = slash pine, longleaf pine 8 = pond pine, shortleaf pine 9 = loblolly pine	ine			For torching trees
*8	Torching tree DBH	in	cm	\	
*9	Torching tree height	ft	m	—]	
*10	Number of trees torching together			/	
*11	Continuous flame height	ft	m		For burning pile
*12	Flame length	ft	m		For wind-driven surface fire May come from DIRECT
DUTPL	JΤ				
	Maximum spot fire distance	mi	km		

^{*}A range of values is allowed.







Andrews, Patricia L.; Chase, Carolyn H. 1989. BEHAVE: fire behavior prediction and fuel modeling system—BURN subsystem, Part 2. Gen. Tech. Rep. INT-260. Ogden, UT: U.S. Department of Agriculture, Forest Service, Intermountain Research Station. 93 p.

This is the third publication describing the BEHAVE system of computer programs for predicting behavior of wildland fires. This publication adds the following predictive capabilities: distance firebrands are lofted ahead of a wind-driven surface fire, probabilities of firebrands igniting spot fires, scorch height of trees, and percentage of tree mortality. The system includes a separate module for graphing moisture content of fine, dead fuels. Basic assumptions, limitations, and application of the prediction models are discussed. Previous publications in the BEHAVE series are BEHAVE: fire behavior prediction and fuel modeling system—FUEL subsystem (Burgan and Rothermel 1984), and BEHAVE: fire behavior prediction and fuel modeling system—BURN subsystem, Part 1 (Andrews 1986).

KEYWORDS: wildland fire, fire management, fire effects, firebrand, fire ignition, tree mortality

INTERMOUNTAIN RESEARCH STATION

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